



Technical Report 1702
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SeaRad, A Sea Radiance Prediction Code

C. R. Zeisse

Naval Command, Control and
Ocean Surveillance Center
RDT&E Division

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ADMINISTRATIVE INFORMATION

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EXECUTIVE SUMMARY

OBJECTIVE

Develop a computer code to predict sea radiance (brightness).

APPROACH

Sea radiance is modeled by combining the methods of geometrical optics with the Cox-Munk statistical description of ocean capillary waves. The model is incorporated into the atmospheric transmittance/radiance code MODTRAN2 to provide numerical sea radiance predictions.

In this model each individual capillary wave facet is allowed to reflect the sky or sun and emit thermal radiation. The total radiance from the sea is obtained by applying the proper statistical weight to each facet and integrating over all facets within the observer's field-of-view.

RESULTS

The modified MODTRAN2 code, called *SeaRad*, calculates sea radiance for any viewing geometry in a spectral range from 52.63 cm^{-1} to 25000 cm^{-1} . Typical execution speeds are approximately 10 s per pixel on a Pentium/90 MHz personal computer. Preliminary comparisons show that *SeaRad* agrees to within several degrees Celsius ($^{\circ}\text{C}$) with actual sea radiance measurements in the mid-wave and long-wave infrared bands.

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1. INTRODUCTION

SeaRad is a FORTRAN computer code that predicts the radiance (brightness) of the ocean surface. *SeaRad* is based on the Cox-Munk statistical model (Cox and Munk, 1954, 1956) for wind-driven capillary wave facets. An individual facet is chosen and assigned a specific slope with respect to the local horizon. The facet is allowed to reflect the sky and sun and emit thermal black body radiation toward an observer. The total radiance is obtained by applying the proper statistical weight to the facet and integrating over all facets within the observer's field-of-view.

SeaRad is valid for a spectral range extending from the visible to the far infrared. Preliminary comparisons show that *SeaRad* agrees to within several °C with actual sea radiance measurements in the mid-wave and long-wave infrared bands.

In its current form, *SeaRad* is a self-contained, DOS-compatible program that runs on a personal computer and computes radiance for a single pixel (rather than an entire image). It is a modified version of the Air Force program MODTRAN2 (Berk, et al., 1989; Kneizys, et al., 1988) that computes atmospheric transmittance and radiance. *SeaRad* operates exactly like the original MODTRAN2 code¹ except that a new logical parameter, "SeaSwitch", is required in the input file. Sun glint is included in the sea radiance prediction provided that the user has chosen to execute *SeaRad* in radiance mode with solar scattered radiance included (IEMSCT = 2).

2. HARDWARE CONSIDERATIONS

The size of the FORTRAN source code is 1.8 MB. When assembled by version 5.01 of the Lahey F77L/EM-32 DOS compiler, the size of the executable code is 0.8 MB. When run² on a Pentium/90 at low spectral resolution (LOWTRAN7) in multiple scattering mode, execution times are 4 s for a typical thermal long-wave case (830 to 1250 cm⁻¹ in 21 spectral steps) and 17 s for a typical solar mid-wave case (2000 to 3340 cm⁻¹ in 67 spectral steps). Source and executable codes are available on disk through correspondence with the author.

3. AN EXAMPLE

This section provides an example of how *SeaRad* is used to predict radiance of the ocean surface. An input file called "Tape5Rad.Std," shown on page A-2, employs a 1976 U. S. standard atmosphere to calculate ocean radiance observed at a zenith angle of 100° (a depression angle of 10°) from a height of 23 m. The Navy aerosol model is used. The calculation is done at low spectral resolution (LOWTRAN7) for a single wave number (945 cm⁻¹) in the long-wave band.

With this file present, the following three DOS commands will calculate ocean radiance and display results:

```
Copy Tape5Rad.Std Tape5
SeaRad
Type Out
```

1 This report assumes that the reader is familiar with MODTRAN2 operation.

2 The compiler requires the Lahey/Phar Lap 386 DOS Extender program (0.2 MB) to run on a personal computer.

These commands³ produce the output file “Out” (Appendix A, page 3). Band-integrated radiance values in $\text{W m}^{-2} \text{ sr}^{-1}$ are listed at the end of the output file for each of four contributions to ocean radiance: path to footprint, sea emission, sky reflection, and sun glint. (In fact, no sun glint has been calculated in this instance since the input file specifies IEMSCT = 1 rather than IEMSCT = 2.) Please note that the parameter “TBOUND” in the input file has been reinterpreted by *SeaRad* as the sea temperature.

The input file shown in Appendix A on page 2 contains two new parameters at the end of the third line: “90.000” and “T”. These will be discussed in reverse order of their appearance.

The “T”, which may appear anywhere in columns 76 through 80 of the third line of the input file (at the end of Card 3), is a new logical parameter “SeaSwitch”. It is required; that is, a fatal error will be generated if it is not present in the input file. “SeaSwitch” controls the sea radiance calculation. When “SeaSwitch” is equal to “T”, the sea radiance calculation will be allowed provided certain other conditions are met. When “SeaSwitch” is equal to “F”, the sea radiance calculation will be prevented under all conditions and the program will execute as originally released by the Air Force.

The “90.000”, which may appear anywhere in columns 66 through 75 of the third line of the input file (near the end of Card 3), is a new floating point parameter, “Psi”. It is optional; that is, the program will run whether this parameter is included in the input file or not. “Psi” is the azimuth of the upwind direction⁴ measured from the line-of-sight in degrees positive East of North. If it is omitted (if the field is blank), and if all conditions for a sea radiance calculation are met, that calculation will proceed under the assumption that the value of “Psi” is zero, meaning that the observer is looking directly into the wind. For the input file in Appendix A, “Psi” is 90°, meaning that the wind is blowing from right to left, perpendicular to the direction of observation.

The modified version of Card 3 used by *SeaRad* is:

```
H1, H2, ANGLE, RANGE, BETA, R0, LEN, Psi, SeaSwitch  
Format (6F10.3, I5, F10.3, L5)
```

4. THE MODEL

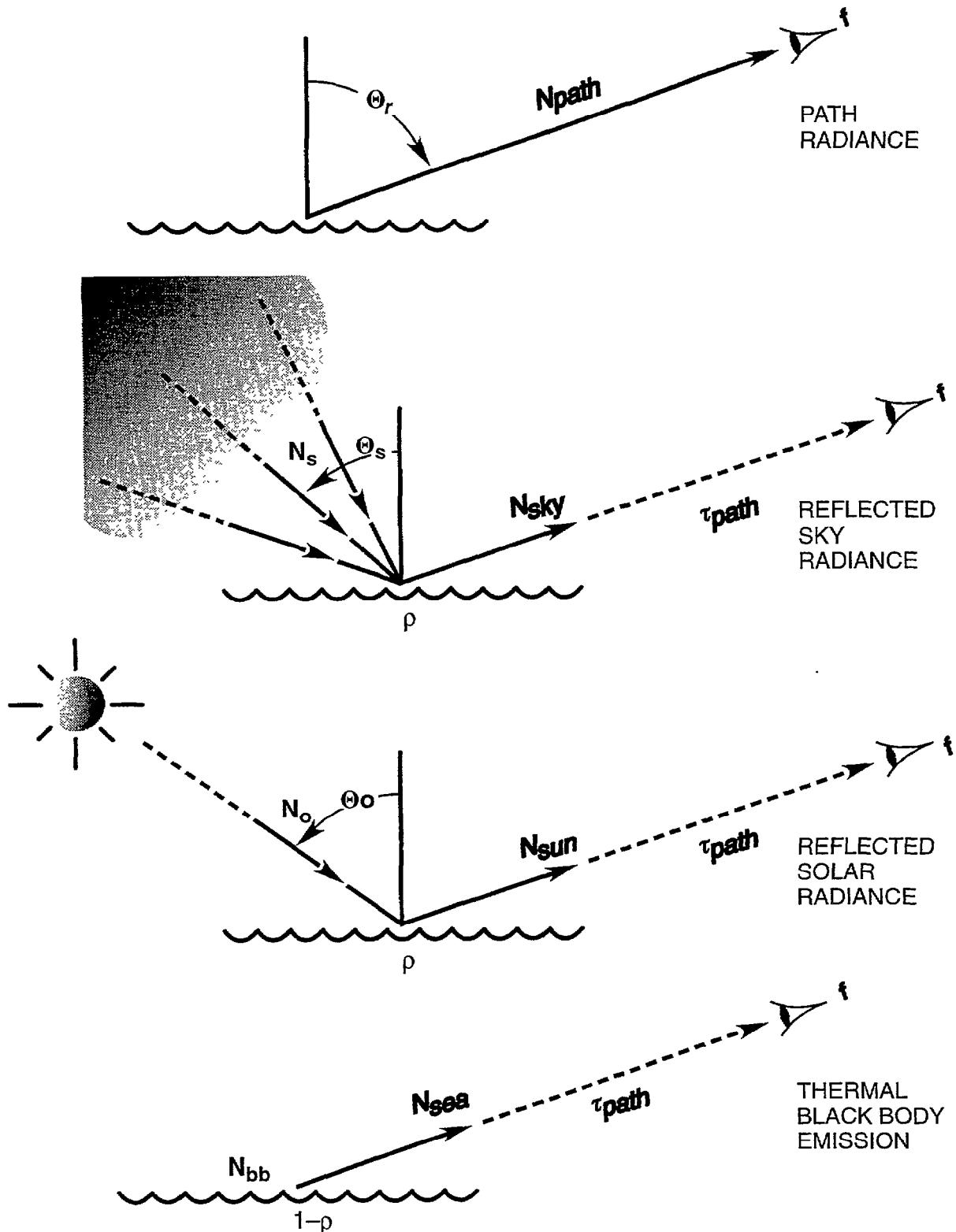
The primary assumption of the model is that the strength of interaction between an optical ray and a capillary wave facet is given by the facet area projected normal to the ray. A feature (Zeisse, 1994. 1995) of the equations contained in *SeaRad* is that they predict a finite horizon radiance. *SeaRad* does not include multiple reflections, shadowing, or gravity waves. Polarization is ignored.

The model computes four contributions to sea radiance. Each of the four contributions is shown in figure 1. (For purposes of clarity, only two dimensions have been used in figure 1; however, all three dimensions are used in the actual calculation.)

The first contribution is path radiance, shown at the top of figure 1. The footprint of a single pixel in an image of the sea is indicated by the wavy line. The footprint is observed by a receiver at the end

3. The time for this particular test case was 3 s on a 486/50 MHz personal computer.

4. This information is required because the Cox-Munk capillary wave slope statistics are different in the upwind and crosswind directions.



$$(N_{\text{sky}} + N_{\text{sun}} + N_{\text{sea}}) \tau_{\text{path}} \cdot f + N_{\text{path}} \cdot f = N$$

Figure 1. Four contributions to sea radiance.

of a ray whose zenith angle at the footprint is θ_r . Let N_{path} designate the spectral radiance in $\text{W m}^{-2} \text{sr}^{-1} (\text{cm}^{-1})^{-1}$ along the path⁵ from the footprint to the receiver.

The second contribution is reflected sky radiance. Spectral radiance N_s from a portion of the sky arrives at the footprint along a ray whose zenith angle there is θ_s . The footprint contains wave facets of different slopes, many that reflect the incoming sky radiance away from the receiver toward other parts of the sky. These facets are ignored. However, the footprint will contain some facets whose slope is correct for reflecting the incoming sky radiance toward the receiver along the path defined by the zenith angle θ_r . These facets are retained. The contributions from all portions of the sky are summed together after specular reflection by the appropriate facets within the footprint, and the sum leaving the footprint at zenith angle θ_r is designated N_{sky} . During its path to the receiver, the reflected sky radiance is attenuated by the path transmission τ_{path} .

The third contribution is reflected solar radiance, sun glint. The calculation is analogous to the calculation of sky radiance. Spectral radiance N_o from the solar center arrives at the footprint along a path whose zenith angle there is θ_o . Within the footprint, most facets deflect the solar ray away from the receiver and are rejected, but some facets are retained because they deflect the ray specularly toward the receiver along a path with zenith angle θ_r . N_{sun} is the spectral radiance leaving the footprint after summation over rays arriving from all portions of the solar disk. The reflected solar radiance is also attenuated by the path transmission τ_{path} before final reception.

The fourth contribution is thermal black body emission. Each facet emits a spectral radiance N_{bb} given by Planck's equation for a black body whose temperature is equal to the value of "TBOUND" in the input file. The spectral emissivity of a given facet in the direction of the receiver is specified by the slope of that facet and the value of θ_r . N_{sea} is the thermal spectral radiance leaving the footprint for the receiver after summation over all facets within the footprint. As before, N_{sea} is attenuated by path transmission after leaving the footprint.

Throughout figure 1, the symbol ρ represents the spectral reflectivity of sea water, which is required for the second and third contributions since they are governed by the process of optical reflection. On the other hand, the fourth contribution is governed by the process of optical emission. Fortunately, by application of Kirchoff's Law to an opaque medium, sea water, the emissivity is given by one minus the reflectivity. The reflectivity is calculated from Fresnel's equations (Stratton, 1941) with a complex optical index taken from the literature (Hale & Querry, 1973; Querry, et al., 1977). These data for the index, available between 52.63 cm^{-1} and 25000 cm^{-1} , set the spectral range of *SeaRad*.

The total spectral radiance N received at wave number v (cm^{-1}) is given by

$$N(v) = N_{path}(v) f(v) + [N_{sky}(v) + N_{sun}(v) + N_{sea}(v)] \tau_{path}(v) f(v), \quad (1)$$

where $f(v)$ has been introduced to represent the spectral responsivity of the receiver.

The design of *SeaRad* is such that path (N_{path}, τ_{path}) and source (N_s, N_o, N_{bb}) values are taken from the original MODTRAN2 while Fresnel reflection (ρ) and slope integrated values ($N_{sky}, N_{sun}, N_{sea}$) are introduced in new subroutines. Integration of (1) over the wave number band specified in the input file is carried out in a modification of subroutine "TRANS" to produce the band-integrated values for sea radiance given in the output file.

5. In this report, the word path refers to only the optical path between the footprint and the receiver.

5. THE COORDINATE SYSTEM

The previous description neglected the azimuthal dependence of rays arriving and leaving the footprint. The full three-dimensional geometry will now be introduced.

Figure 2 shows the geometry of reflection. A coordinate system was chosen whose origin is the point of reflection with the X-axis pointing upwind, the Z-axis pointing toward the zenith, and the Y-axis pointing crosswind such that a right-handed system is formed. The X-Y plane is horizontal at the point of reflection. The tilted facet passes through the origin.

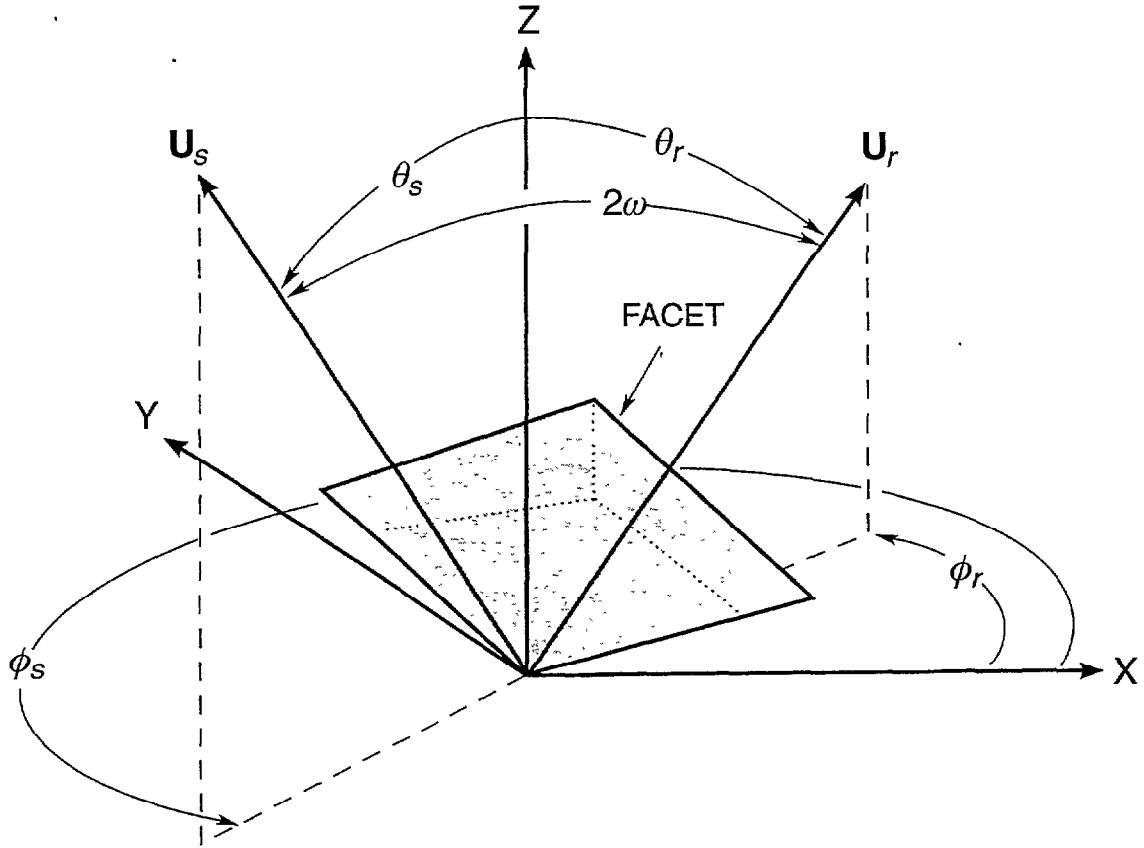


Figure 2. Coordinate system for facet reflection.

Define a unit vector $\mathbf{U} \equiv (\theta, \phi)$ with polar coordinates θ , the zenith angle, and ϕ , the azimuth. If we denote the Cartesian coordinates of \mathbf{U} by (a, b, c) , then we have

$$\begin{aligned} a &= \sin \theta \cos \phi \\ b &= \sin \theta \sin \phi \\ c &= \cos \theta \end{aligned} \tag{2}$$

for the Cartesian coordinates of \mathbf{U} in terms of its spherical coordinates and

$$\begin{aligned} \theta &= \cos^{-1}(c) \\ \phi &= \tan^{-1}(b/a) \end{aligned} \tag{3}$$

for the spherical coordinates of \mathbf{U} in terms of its Cartesian coordinates. Two unit vectors are shown in figure 2: \mathbf{U}_s , pointing from the origin to the source, and \mathbf{U}_r , pointing from the origin to the receiver. A third unit vector, \mathbf{U}_n , is normal to the facet at the point of reflection but was removed from the figure for clarity⁶.

The facet slope in the upwind direction, ζ_x , is given by the slope of the line formed at the intersection of the facet with the X - Z plane. The facet slope in the crosswind direction, ζ_y , is given by the slope of the line formed at the intersection of the facet with the Y - Z plane. In terms of the Cartesian coordinates of the facet normal these slopes are

$$\begin{aligned}\zeta_x &= -a_n/c_n \\ \zeta_y &= -b_n/c_n\end{aligned}\tag{4}$$

6. SPECULAR REFLECTION

If a specular reflection occurs, the three vectors for source, receiver, and facet normal are connected by the law of reflection:

$$\mathbf{U}_s + \mathbf{U}_r = 2 \cos \omega \mathbf{U}_n\tag{5}$$

where ω is the angle of incidence and the angle of reflection.

7. THE OCCURRENCE PROBABILITY

Following Cox and Munk, let P stand for the probability

$$P \equiv p(\zeta_x, \zeta_y, W) d\zeta_x d\zeta_y\tag{6}$$

that a wave facet will occur with a slope within $\pm d\zeta_x/2$ of ζ_x and $\pm d\zeta_y/2$ of ζ_y when the wind speed is W . The wave slope occurrence probability density, p , is proportional to the horizontal projection of the facet. Cox and Munk obtained an expression for p whose lowest order term is

$$\begin{aligned}p(\zeta_x, \zeta_y, W) &\approx \frac{1}{2\pi\sigma_u\sigma_c} \exp \left\{ -\frac{1}{2} \left(\frac{\zeta_x^2}{\sigma_u^2} + \frac{\zeta_y^2}{\sigma_c^2} \right) \right\} \\ \sigma_u^2 &= 0.000 + 3.16 \cdot 10^{-3}W \\ \sigma_c^2 &= 0.003 + 1.92 \cdot 10^{-3}W\end{aligned}\tag{7}$$

Here σ_u^2 and σ_c^2 are the variances in ζ_x and ζ_y respectively and W is the wind speed in m s^{-1} . Figure 3 shows the dependence of p throughout slope space for a wind speed of 10 m s^{-1} . The coordinate system of figure 2 has been inserted at the top of the figure to illustrate the relation between coordinates and slopes. Note that the first X - Y quadrant corresponds to negative slopes.

6. The zenith angle of \mathbf{U}_n is the same as the tilt of the facet. The tilt is the angle of the steepest ascent within the facet.

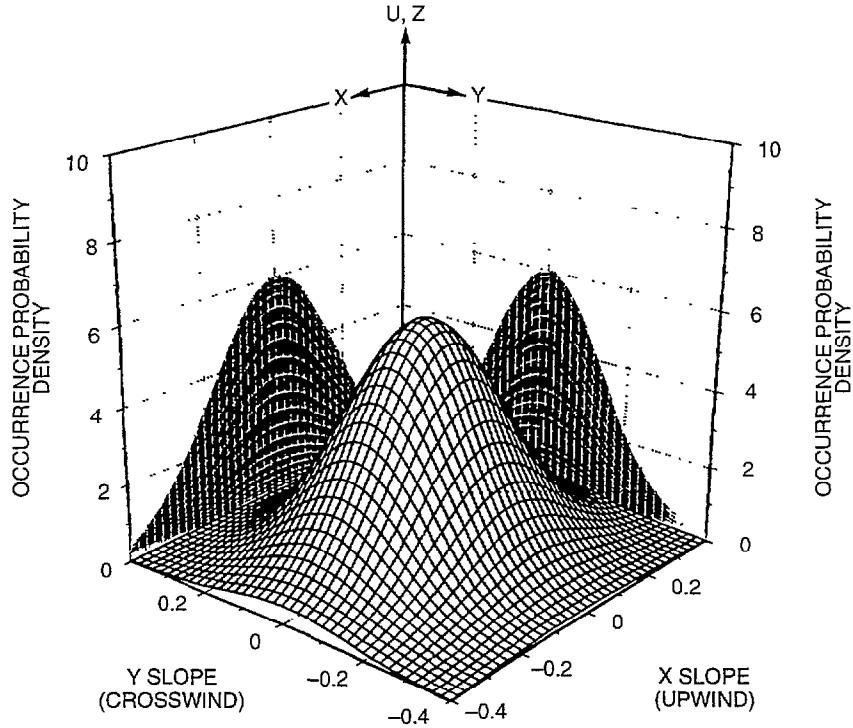


Figure 3. Cox-Munk occurrence probability density for a windspeed of 10 m s^{-1} .

8. THE INTERACTION PROBABILITY

Following a suggestion of Plass, et al. (1976), let Q stand for the (different) probability

$$Q \equiv q(\xi_x, \xi_y, \theta, \phi, W) \xi_x d\xi_y \quad (8)$$

that a facet whose slope is within $\pm d\xi_x/2$ of ξ_x and $\pm d\xi_y/2$ of ξ_y will interact with a ray arriving from the arbitrary direction $\mathbf{U} = (\theta, \phi)$ when the wind speed is W . The wave slope interaction probability density, q , is proportional to the facet area projected normal to the ray. It has previously been shown (Zeisse, 1994, 1995)⁷ that

$$q(\xi_x, \xi_y, \theta, \phi, W) = \frac{\frac{\cos \omega}{\cos \theta_n} p}{\iint_{\substack{\omega \leq \pi/2 \\ U = \text{const}}} \frac{\cos \omega}{\cos \theta_n} p d\xi_x d\xi_y} \quad (9)$$

Figure 4 is a graph of equation (9), also for a wind speed of 10 m s^{-1} , showing how facets with a specified slope interact with a ray pointing in the direction $(80^\circ, 270^\circ)$.

7. Equation (9) is only defined for $\omega \leq \frac{\pi}{2}$.

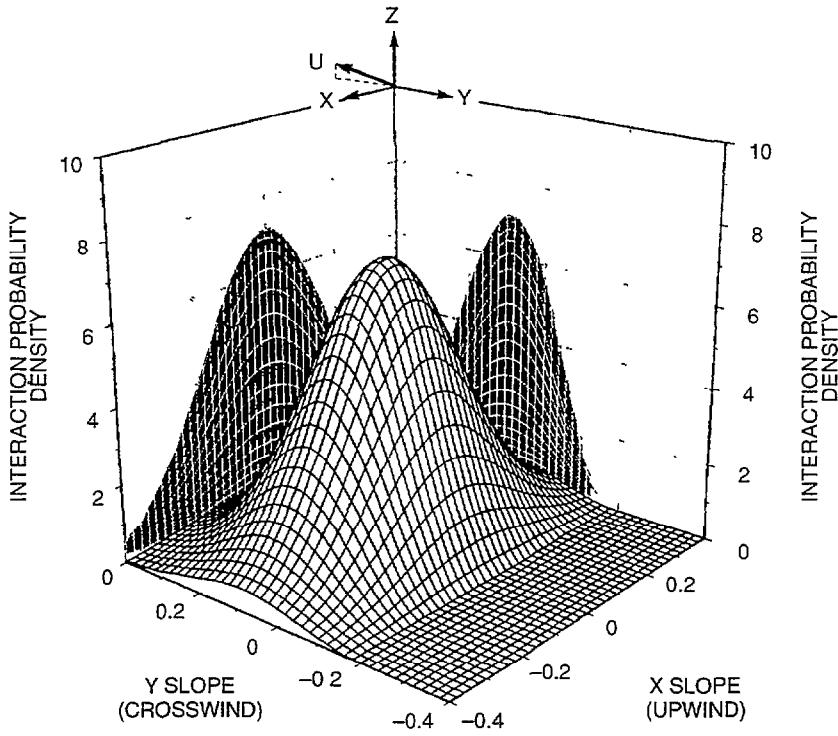


Figure 4. Cox-Munk-Plass interaction probability density for a windspeed of 10 m s^{-1} .

9. EQUATIONS FOR SEA RADIANCE

The capillary wave contributions to sea radiance are

$$N_{sky}(\theta_r, \phi_r, W, v) = \int \int_{\substack{\theta_s, \omega \leq \pi/2 \\ U_r = \text{const.}}} N_s(\theta_s, \phi_s, v) \rho(\omega, v) q(\xi_x, \xi_y, \theta_r, \phi_r, W) d\xi_x d\xi_y \quad (10)$$

$$N_{sun}(\theta_o, \phi_o, \theta_r, \phi_r, W, v) \approx \frac{N_o(\theta_o, \phi_o, v)}{4}. \quad (11)$$

$$\int \int_{\substack{disk \\ U_r = \text{const.}}} \rho(\omega, v) \sec \omega \ sec^3 \theta_n q(\xi_x, \xi_y, \theta_r, \phi_r, W) \ sin \theta_s d\theta_s d\phi_s$$

$$N_{sea}(\theta_r, \phi_r, W, T_{sea}, v) = N_{bb}(T_{sea}, v) \int \int_{\substack{\omega \leq \pi/2 \\ U_r = \text{const.}}} [1 - \rho(\omega, v)] q(\xi_x, \xi_y, \theta_r, \phi_r, W) d\xi_x d\xi_y \quad (12)$$

In each of the integrals (10) through (12), q plays the role of a weighting function attached to the facet. The weight is applied to the ray leaving the footprint and propagating toward the receiver, and

that ray and those receiver coordinates are held constant in all of the integrals. A physical description and some mathematical details of each equation will now be presented.

In the integrand of (10), the product of N_s and ρ represents the radiance leaving a single facet when $N_s(\theta_s, \phi_s, \nu)$ is the spectral sky radiance incident on that facet at zenith angle θ_s and azimuth ϕ_s . This product is weighted by q and integrated over all slopes in the ocean. During integration, a specular reflection occurs at one facet after another inside the footprint with the outgoing (receiver) ray held fixed. The source ray is swept across the sky and sun. Equation (10) will require explicit expressions for each of its variables in terms of slopes and receiver coordinates. From (2) and (4) it can be shown that the facet tilt is given in terms of the facet slopes by

$$\cos \theta_n = c_n = \frac{1}{\sqrt{1 + \xi_x^2 + \xi_y^2}} \quad (13)$$

while the fact that ω is the angle between the facet normal and the receiver ray implies that

$$\begin{aligned} \cos \omega &= \mathbf{U}_n \cdot \mathbf{U}_r \\ &= a_n a_r + b_n b_r + c_n c_r \\ &= \{-\xi_x a_r - \xi_y b_r + c_r\} c_n \\ &= \frac{\{-\xi_x \sin \theta_r \cos \phi_r - \xi_y \sin \theta_r \sin \phi_r + \cos \theta_r\}}{\sqrt{1 + \xi_x^2 + \xi_y^2}} \end{aligned} \quad (14)$$

Equations (13) and (14) hold at all times, regardless of whether a specular reflection is taking place. When a specular reflection does occur, the Z component of the law of reflection

$$\mathbf{U}_s = 2 \cos \omega \mathbf{U}_n - \mathbf{U}_r \quad (15)$$

gives

$$\begin{aligned} \cos \theta_s &= 2 \cos \omega c_n - c_r \\ &= \frac{2\{\} - c_r/c_n^2}{1/c_n^2} \\ &= \frac{-2 \sin \theta_r (\xi_x \cos \phi_r + \xi_y \sin \phi_r) + \cos \theta_r (1 - \xi_x^2 - \xi_y^2)}{1 + \xi_x^2 + \xi_y^2} \end{aligned} \quad (16)$$

where $\{\}$ represents the expression within curly braces in (14). Finally, the X and Y components of (15) give

$$\begin{aligned} \tan \phi_s &= \frac{b_s}{a_s} \\ &= \frac{2 \cos \omega b_n - b_r}{2 \cos \omega a_n - a_r} \\ &= \frac{2\xi_y \{\} + b_r/c_n^2}{2\xi_y \{\} + a_r/c_n^2} \\ &= \frac{(1 + \xi_x^2 - \xi_y^2) \sin \phi_r - (2\xi_x \xi_y) \cos \phi_r + (2\xi_y) \cot \theta_r}{(1 - \xi_x^2 + \xi_y^2) \cos \phi_r - (2\xi_x \xi_y) \sin \phi_r + (2\xi_x) \cot \theta_r} \end{aligned} \quad (17)$$

for the source azimuth during specular reflection by a facet (ξ_x, ξ_y) into a receiver at (θ_r, ϕ_r) .

Equations (13), (14), (16), and (17) should be used in (10) [and in equation(9) when using (10)]. The Cartesian expressions are convenient for computer calculation while the spherical expressions are consistent with the form of equations (10) through (12).

In the integrand of (11), the product of N_o and ρ represents the spectral radiance leaving a single facet when $N_o(\theta_o, \phi_o, \nu)$ is the spectral radiance arriving at that facet from the sun whose center is at (θ_o, ϕ_o) . The remaining factors in (11), apart from q , are the Jacobian of the transformation from ocean slopes to sky coordinates (Zeisse, 1994). As before, the integrand is weighted by q but now the integration is over the solar disk in the sky. (It is assumed in (11) that $N_o(\theta_o, \phi_o, \nu)$ does not vary during integration because the sun is a Lambertian source and the solar disk is small.) During integration, a specular reflection from the sun to the receiver occurs at those facets within the footprint with the correct slope. Explicit expressions for each of the variables in terms of source and receiver coordinates will be required in (11). The law of reflection

$$2 \cos \omega \mathbf{U}_n = \mathbf{U}_s + \mathbf{U}_r \quad (18)$$

gives the facet position in terms of the source and receiver positions whenever a specular reflection occurs. The components of (18) give

$$\begin{aligned} \xi_x &= -\frac{a_n}{c_n} \\ &= -\frac{a_s + a_r}{c_s + c_r} \\ &= -\frac{\sin\theta_s \cos\phi_s + \sin\theta_r \cos\phi_r}{\cos\theta_s + \cos\theta_r} \end{aligned} \quad (19)$$

and

$$\begin{aligned} \xi_y &= -\frac{b_n}{c_n} \\ &= -\frac{b_s + b_r}{c_s + c_r} \\ &= -\frac{\sin\theta_s \sin\phi_s + \sin\theta_r \sin\phi_r}{\cos\theta_s + \cos\theta_r} \end{aligned} \quad (20)$$

while its square gives

$$\begin{aligned} 2 \cos^2 \omega &= 1 + \mathbf{U}_s \cdot \mathbf{U}_r \\ &= 1 + a_s a_r + b_s b_r + c_s c_r \\ &= 1 + \sin\theta_s \sin\theta_r \cos(\phi_s - \phi_r) + \cos\theta_s \cos\theta_r \end{aligned} \quad (21)$$

Finally, from (2), (4), and (18) we have

$$\begin{aligned}
 \tan^2 \theta_n &= \zeta_x^2 + \zeta_y^2 \\
 &= \frac{(a_s + a_r)^2 + (b_s + b_r)^2}{(c_s + c_r)^2} \\
 &= \frac{\sin^2 \theta_s + \sin^2 \theta_r + 2 \sin \theta_s \sin \theta_r \cos(\phi_s - \phi_r)}{(\cos \theta_s + \cos \theta_r)^2}
 \end{aligned} \tag{22}$$

Expressions (19) through (22) should be used in (11) [and in (9) when using (11)]. They apply only when there is a specular reflection.

In (12) there is no incident ray or specular reflection, and integration is over all slopes in the ocean. The integral in (12) is the effective spectral emissivity of the ocean. Explicit expressions in terms of slopes and receiver coordinates will also be required for each of the variables in (12) [and in (9) when using (12)]. Equation (13) is the expression for θ_n and equation (14) is the expression for ω .

10. ***SEARAD***

SeaRad consists of new routines added to MODTRAN2 to compute the spectral values of N_{sky} , N_{sun} , and N_{sea} according to equations (10), (11), and (12), respectively. Through modifications to subroutine "TRANS", these values are assembled according to (1) and integrated over the wave number after obtaining proper path radiance and transmittance spectral values. *SeaRad* also introduces minor changes in subroutine "DPFNMN" and major changes in subroutine "DRIVER". These changes will now be considered in more detail.

The modifications to "DRIVER" are briefly shown in figure 5. After the normal call to "GEO", a test is conducted to see whether the ray chosen by the user has hit the surface of the sea. If so, geometry cards required for the sea calculation are issued by subroutine "Card" to file "Tape5.Sea", and input is temporarily redirected to "Tape5.Sea". An example of "Tape5.Sea" is given on page A-4, for the run initiated by the input file on page A-2. After the final card has been read from "Tape5.Sea", sea radiance is calculated in "TRANS". Then "TAPE5" is restored as the active input file and normal program execution is resumed. Please see Appendix B for a detailed flowchart of the modifications to "DRIVER" as well as the complete source code for the modified version of "DRIVER".

Conditions in "DPFNMN" determine whether or not the sea has been hit. "DPFNMN" is a subroutine reached by a sequence of calls beginning in the driver with a call to subroutine "GEO". Modifications to "DPFNMN" are summarized in figure 6. A logical variable "Sea", initially set false, is set true in "DPFNMN" if the following four conditions are met:

1. The program has reached the section of code following the comment line "Tangent path intersects earth."
2. The user has chosen a radiance mode.
3. The variable "HMIN" is equal to zero.
4. The variable "SeaSwitch" is true.

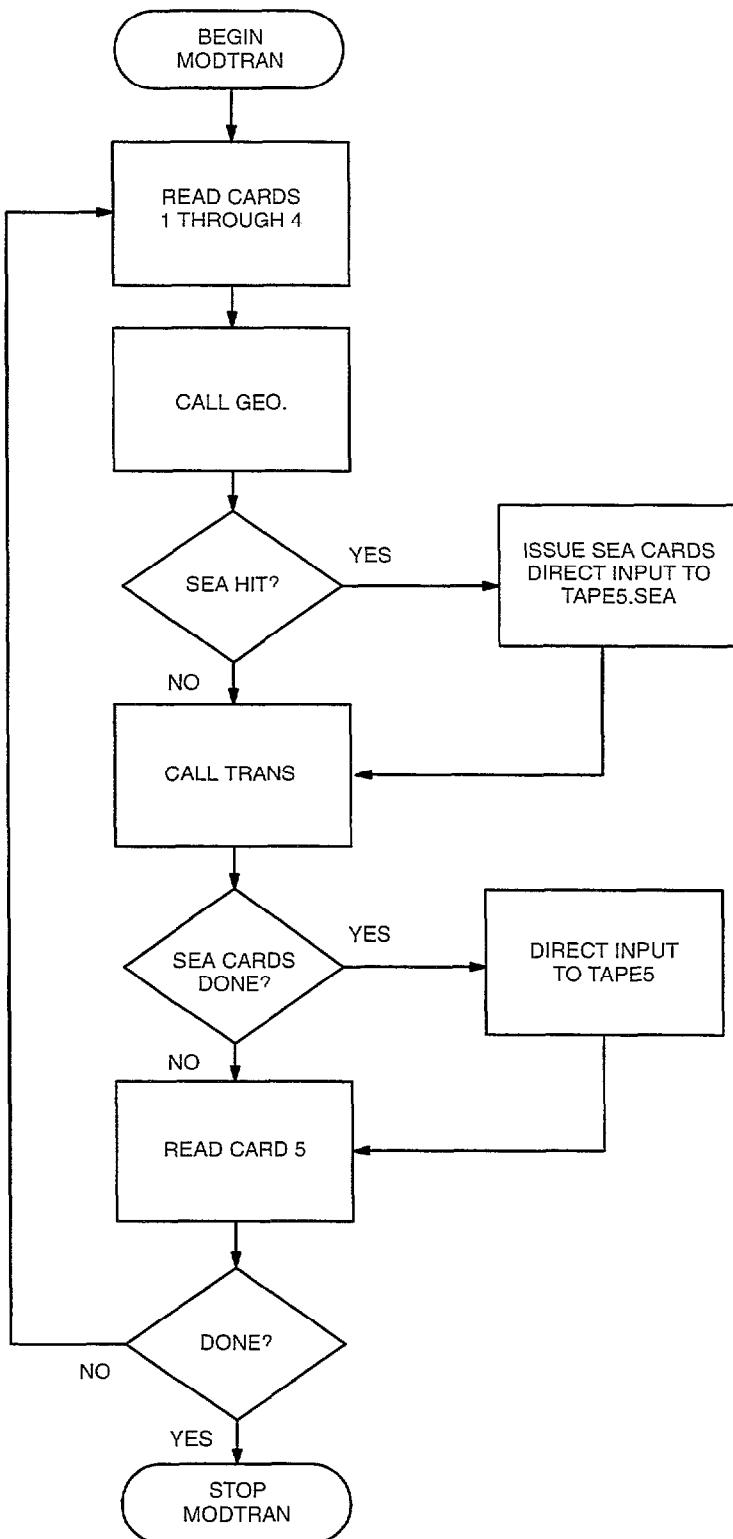


Figure 5. Flowchart for modifications to MODTRAN2 subroutine "DRIVER."

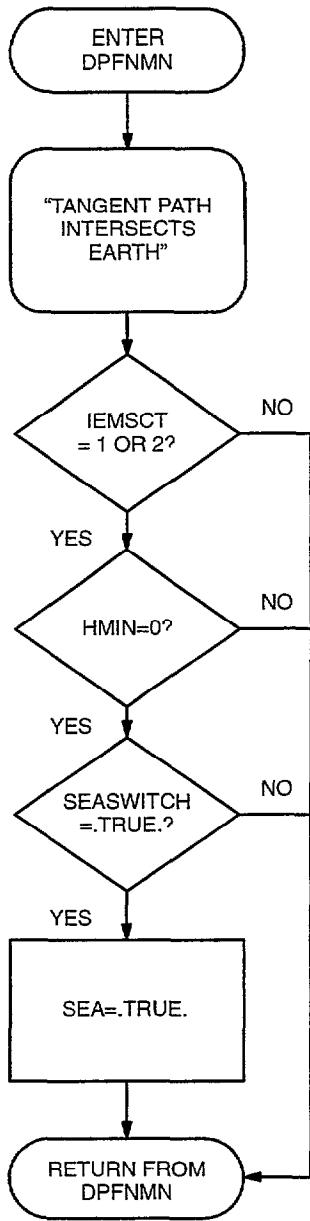


Figure 6. Flowchart for modifications to MODTRAN2 subroutine “DPFNMN.”

The variable “Sea” is stored in a common block made available to the driver, which inspects “Sea” before and after each of its calls to “GEO”. A change from false to true indicates that the ocean has been hit during that call. A hit induces a geometry calculation by a call to subroutine “Foot” (if $IEMSCT = 1$) or subroutine “SunFoot” (if $IEMSCT = 2$). This is followed in each case by a call to subroutine “Card”.

The purpose of “Card” is to supply sources for the Cox-Munk routines “Sky” and “Sun.” As shown in figure 7, geometry cards are issued here to file “Tape5.Sea” to obtain spectral radiance along paths to the sky at three separate zenith angles. These three cards, one for each zenith angle, are called “Sky Cards” in the flowchart. Later these data will be used by subroutine “Fit” to establish a two-parameter least squares fit at each wave number providing “Sky” with the sky dome radiance.

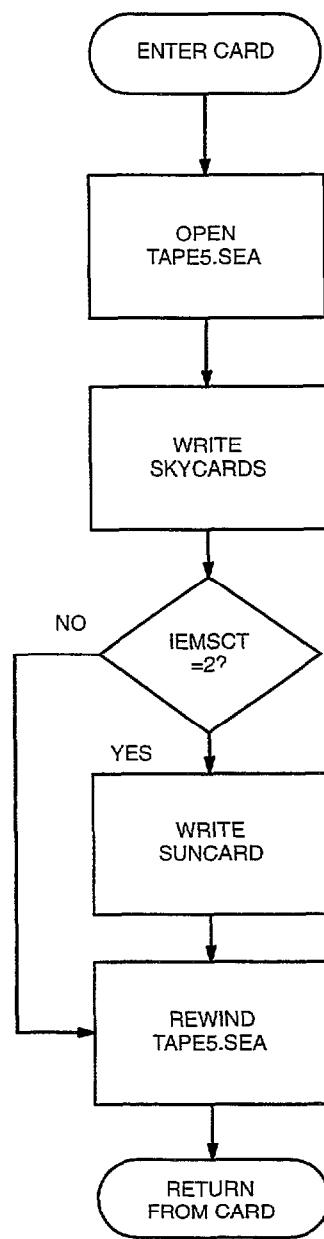


Figure 7. Flowchart for
SeaRad subroutine "Card."

If the sun is involved, “Card” will issue a fourth and final Card 3, called a “Sun Card” in the flowchart, which provides solar irradiance for later use as a source by subroutine “Sun”.

The modifications described to this point have, in effect, inserted three sky cards (followed by a sun card if necessary) into the user’s input file without the user’s knowledge. The insertion is made only if the user has chosen a Card 3 whose path terminates on the surface of the earth. Such a Card 3 is called a “Path Card” in figure C-1. Within the wave number integration loop in “TRANS”, spectral values of transmission, incident sky radiance, and incident solar irradiance are stored in arrays Tau(V), Nsky(V), and Ho(V), respectively. Outside the wave number integration loop these values are recalled for the sea radiance calculation by subroutine “Sky” (or subroutine “Sun” if IEMSCT = 2).

The modified version of “DRIVER” is contained in Appendix B along with a detailed flowchart of its modifications. Appendix C contains the source code and a flowchart for the modified version of “TRANS”, and Appendix D contains new code for the sea radiance calculation.

11. CONCLUSION

SeaRad, a modification of MODTRAN2, computes sea radiance between 52.63 cm^{-1} and 25000 cm^{-1} . Preliminary comparisons with data show that *SeaRad* has an approximate accuracy of several $^{\circ}\text{C}$ in the infrared.

SeaRad is currently designed for a single pixel and takes approximately 10 s to execute. Each time a new geometry is chosen by the user, *SeaRad* recalculates the source radiance and the path radiance and transmission. However, only the path properties change significantly from one pixel to the next in a typical ocean image. If *SeaRad* were redesigned to apply to sea images, the speed per pixel could be reduced, up to a factor of almost four, by calculating values of source radiance just once for the entire image.

12. REFERENCES

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APPENDIX A
***SeaRad* INPUT AND OUTPUT FILES**

"TAPE5RAD.STD" INPUT FILE

C:\MOD2\TAPE5RAD.FIL 7/20/95

F	6	3	1	1	0	0	0	0	0	0	0	0	288.15	0.00
3	0	0	5	0	0	10.000	10.000	10.000	10.000	.000	.000	.000	.000	
00.023	.000	100.000	.000	.000	.000	0.00	0	90.000	T					
	940	950		10		5								
0														

“OUT” FILE

C:\MOD2\OUT.FIL 7/20/95

***** SEARAD, A MODIFICATION OF LOWTRAN7 *****

DATE: 07/20/95

TIME: 15:11:38

THERMAL RADIANCE MODE

MULTIPLE SCATTERING USED

MARINE AEROSOL MODEL USED

WIND SPEED	=	10.00 M/SEC
WIND SPEED	=	10.00 M/SEC, 24 HR AVERAGE
RELATIVE HUMIDITY	=	50.00 PERCENT
AIRMASS CHARACTER	=	5
VISIBILITY	=	10.00 KM

SLANT PATH TO SPACE

H1	=	0.023 KM
HMIN	=	0.000 KM
ANGLE	=	100.000 DEG

FREQUENCY RANGE

IV1	=	940 CM-1 (10.64 MICROMETERS)
IV2	=	950 CM-1 (10.53 MICROMETERS)
IDV	=	10 CM-1
IFWHM	=	5 CM-1
IFILTER	=	0

SUMMARY OF THE GEOMETRY CALCULATION

H1	=	0.023 KM
H2	=	0.000 KM
ANGLE	=	100.000 DEG
RANGE	=	0.133 KM
BETA	=	0.001 DEG
PHI	=	80.001 DEG
HMIN	=	0.000 KM
BENDING	=	0.000 DEG
LEN	=	0

SEA AT 288.15 K REPLACES BLACK BODY BOUNDARY

UPWIND = 90.000 DEG EAST OF LINE OF SIGHT

RECEIVED RADIANCE VALUES

PATH TO FOOTPRINT	=	0.01814 W M-2 SR-1 (AV. TRANS. 0.9776)
SEA EMISSION	=	0.70712 W M-2 SR-1
SKY REFLECTION	=	0.06125 W M-2 SR-1
SUN GLINT	=	0.00000 W M-2 SR-1
TOTAL RADIANCE	=	0.78652 W M-2 SR-1
BLACK BODY TEMP.	=	6.7 C

"TAPE5.SEA" FILE

C:\MOD2\TAPE5SEA.FIL 7/20/95

3	0.000	0.000	57.296	0.000	0.000	0.000	0	90.000	T
3	0.000	0.000	73.148	0.000	0.000	0.000	0	90.000	T
3	0.000	0.000	89.000	0.000	0.000	0.000	0	90.000	T

APPENDIX B
MODIFIED SUBROUTINE “DRIVER”

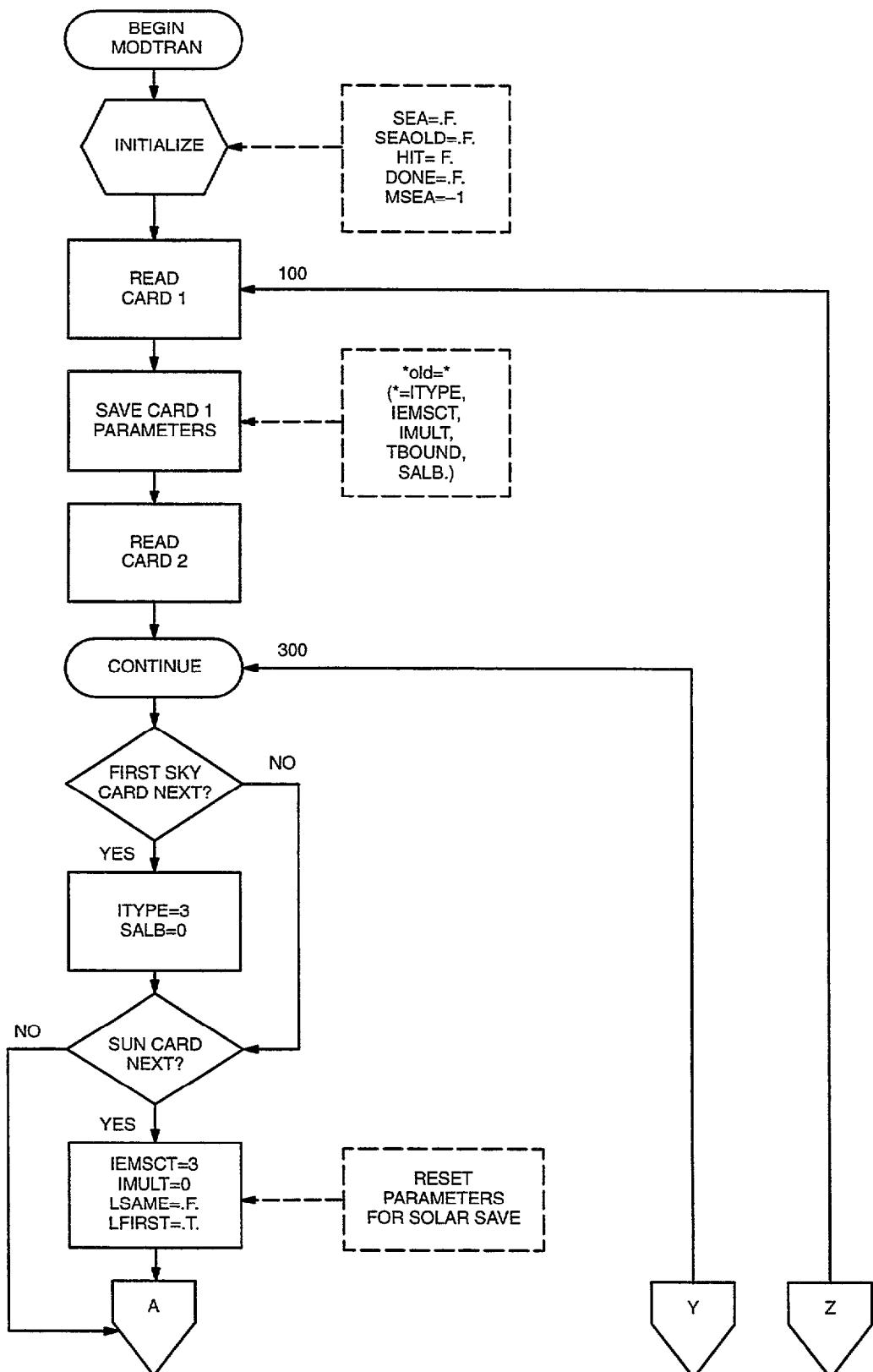


Figure B-1. Detailed flowchart for modified subroutine "DRIVER".

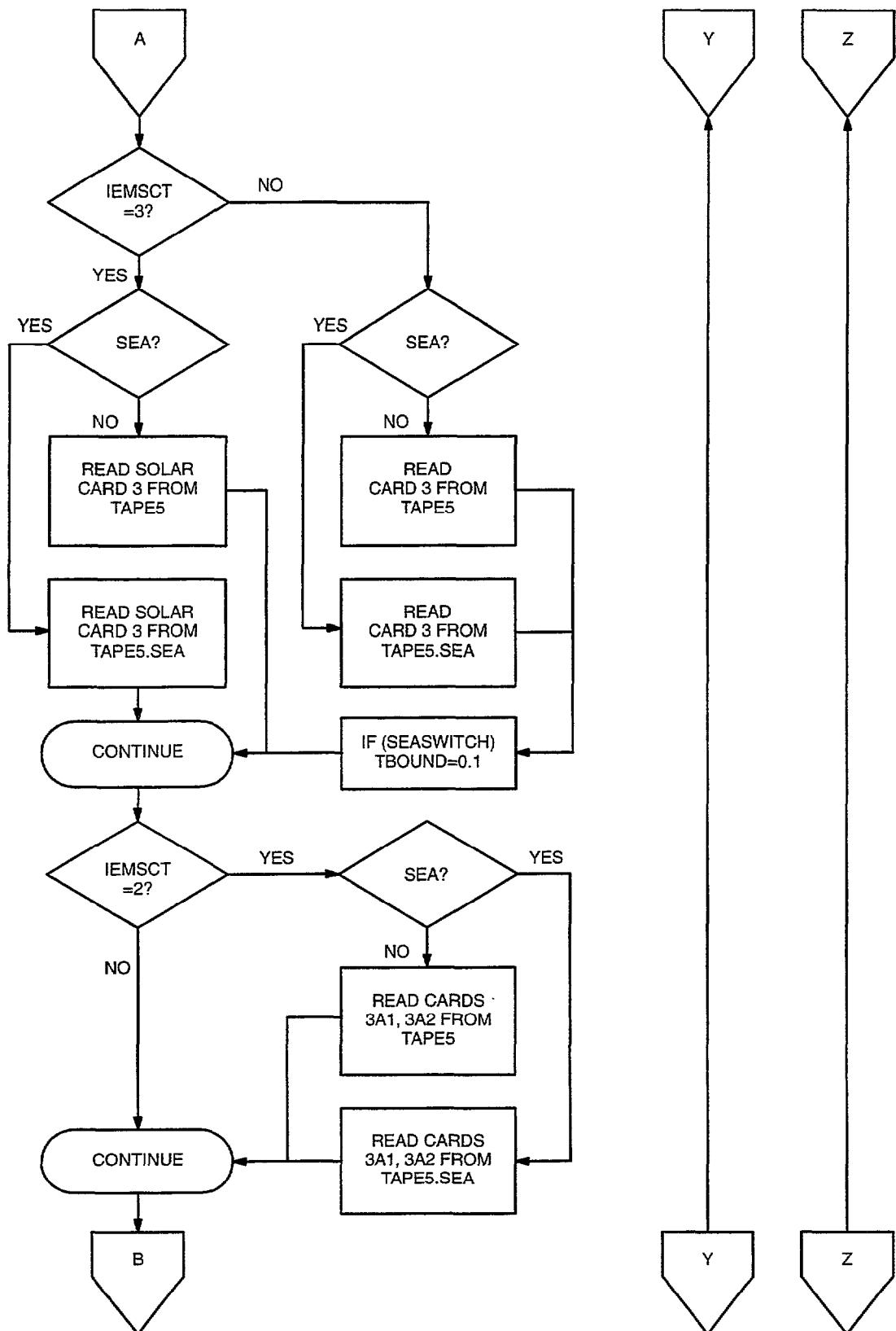


Figure B-1. Detailed flowchart for modified subroutine "DRIVER". (Continued)

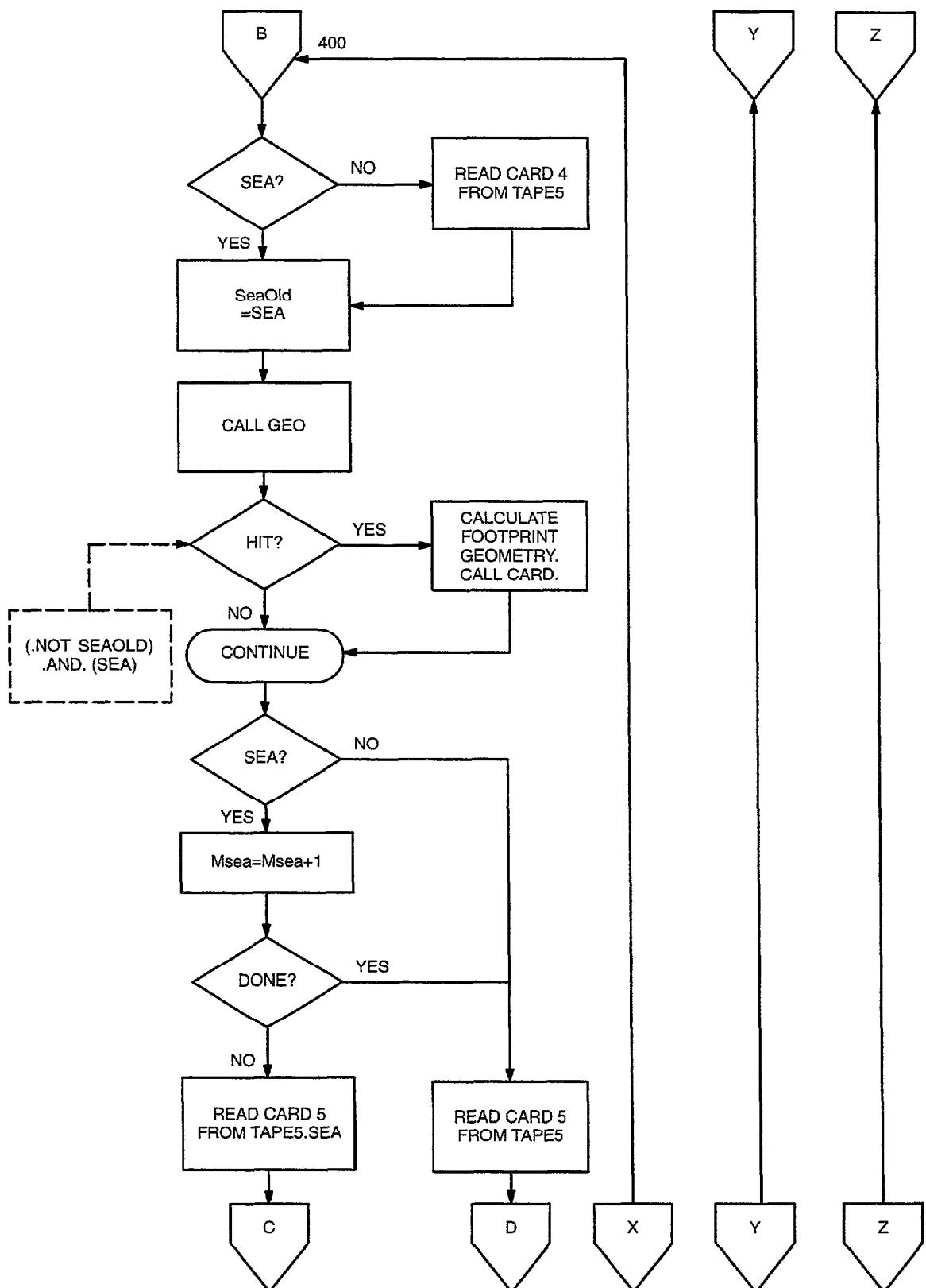


Figure B-1. Detailed flowchart for modified subroutine "DRIVER". (Continued)

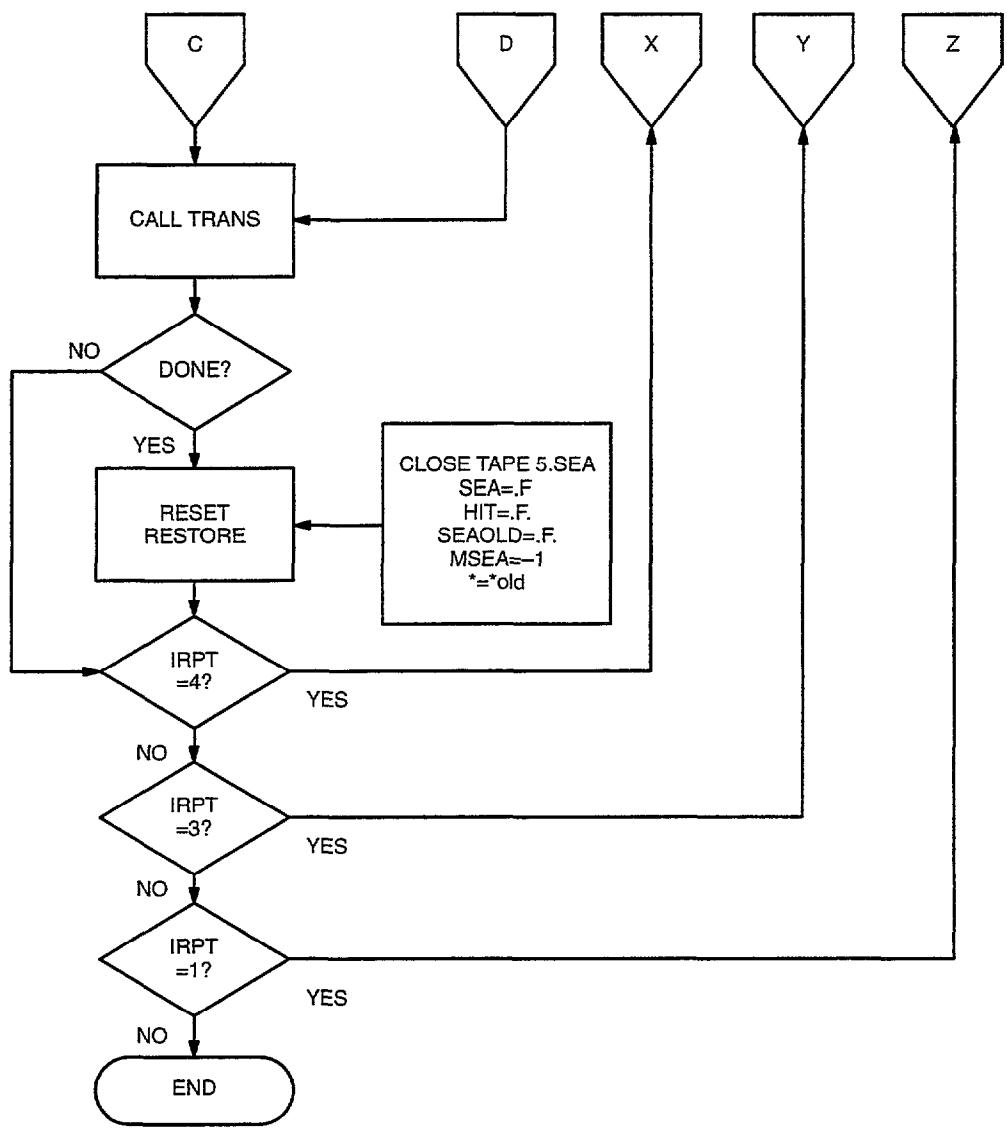


Figure B-1. Detailed flowchart for modified subroutine “DRIVER”. (Continued)

```

SUBROUTINE DRIVER                                driv 100
COMMON RELHUM(34),HSTOR(34),ICH(4),VH(17),TX(63),W(63)   driv 110
C COMMON WPATH(68, 63),TBBY(68)                  driv 120
COMMON IMSMX,WPATH(102,63),TBBY(102),PATM(102),NSPEC,KPOINT(12) driv 130
COMMON ABSC(5,47),EXTC(5,47),ASYM(5,47),VX2(47),AWCCON(5)   driv 140
COMMON /IFIL/ IRD,IPR,IPU,NPR,IPR1,IP6,IP7,IP8,IP4,IRDS,IP6S,ITR,
+           Isky,Isun,Ipath                         driv 160
COMMON /CARD1/ MODEL,ITYPE,IEMSCT,M1,M2,M3,IM,NOPRT,TBOUND,SALB   driv 170
1 ,MODTRN                                         driv 180
LOGICAL MODTRN
logical ground                                     driv 190
logical lsame                                      driv 200
LOGICAL SeaSwitch,Sea,SeaOld,Hit,Done
COMMON /CARD1A/ M4,M5,M6,MDEF,IRD1,IRD2          driv 210
COMMON /CARD2/ IHAZE,ISEASN,IVULCN,ICSTL,ICLD,IVSA,VIS,WSS,WHH,   driv 220
1 RAINRT                                         driv 230
COMMON /CARD2A/ CTHIK,CALT,CEXT                 driv 240
COMMON /CARD2D/ IREG(4),ALTB(4),IREGC(4)        driv 250
COMMON /CARD3/ H1,H2,ANGLE,RANGE,BETA,RE,LEN,Psi,SeaSwitch
COMMON /Card3A1/ IPARM,IPH,IDAY,ISOURC
COMMON /Card3A2/ PARM1,PARM2,PARM3,PARM4,GMT,PSIPO,ANGLEM,G
COMMON /CARD4/ IV1,IV2,IDV,IFWHM,IFILTER
COMMON /CNSTNS/ PIX,CA,DEG,GCAIR,BIGNUM,BIGEXP   driv 290
COMMON /CNTRL/ KMAX,M,IKMAX,NL,ML,IKLO,ISSGEO,IMULT   driv 300
COMMON /MODEL/ ZM(34),PM(34),TM(34),RFNDX(34),DENSTY(63,34),
1 CLDAMT(34),RRAMT(34),EQLWC(34),HAZEC(34)      driv 310
COMMON /SOLS/ AH1(68),ARH(68),                   driv 320
1 WPATHS(102,63),PA(68),PRX(68),ATHETA(35),ADBETA(35),LJ(69),   driv 330
2 JTURN,ANGSUN,CSZEN(68),TBBYS(102,12),PATMS(102,12)
COMMON /MART/ RHH                                 driv 370
COMMON /USRDTA/ NANGL,ANGF(50),F(4,50)          driv 380
COMMON /MDLZ/ HMDLZ(8)                           driv 390
COMMON /ZVSALY/ ZVSA(10),RHVSA(10),AHVSA(10),IHVSA(10)   driv 400
CHARACTER*4 HHAZE,HSEASN,HVULCN,BLANK,HMET,HMODEL,HTRRAD
COMMON /TITL/ HHAZE(5,16),HSEASN(5,2),HVULCN(5,8),BLANK,
1 HMET(5,2),HMODEL(5,8),HTRRAD(6,4)            driv 410
COMMON /VSBD/ VSB(10)                           driv 420
C COMMON /MNLT/TBSS(68),TBBMS(34),WPMS(34,63),IMSMX,WPMSS(34,63)  driv 430
COMMON /PATH/PL(68),QTHETA(68),ITEST,HI,HF,AHT(68),tph(68)    driv 440
COMMON /AERTM/TAE7,TAE12,TAE13,TAE14,TAE16
common /graund/gndalt
common /small3/small
common /solar/lsame
PARAMETER (Kr = 216, Kv = 400)
COMMON /Filters/ FLIST(5,6),
+           FILTER1(45), BB1(Kr), FILTER2(54), BB2(Kr),
+           FILTER3(39), BB3(Kr), FILTER4(47), BB4(Kr),
+           FILTER5(101),BB5(Kr), FILTER6(75), BB6(Kr)
COMMON /Constants/ pi,r2d,d2r,epsilon,delta,onem,onep,infinity
COMMON /Geometry/ Tsun,Psun,Tr,Pr
COMMON /Sea/ Sea,Hit,Msea,TBOUNDold,IEMSCTold
COMMON /SeaIndex/ Alpha01(100),Alpha02(20),
+           Beta01 (100),Beta02 (20)
logical lfist                                     driv 530
data lfist/.true./
REAL infinity
CHARACTER*8 Date$, Time$                         driv 540

```

```

CHARACTER*14 Prog$
INTEGER*4 Istart, Iend
C First, get starting time to measure total execution time:
CALL TIMER(Istart)

C
C Ifirst is true when first solar parameters are read in a series
C of runs involving solar parameters.
C

C*****HDATE AND HTIME CARRY THE DATA AND TIME AND MUST BE DOUBLE
C*****PRECISION ON A 32 BIT WORD COMPUTER
C@ DOUBLE PRECISION HDATE,HTIME
DIMENSION PLST(68),CSENSV(68),QTHETS(68)
DATA IRPT / 0 /
C*****IRD, IPR, AND IPU ARE UNIT NUMBERS FOR INPUT, OUTPUT, AND
C*****IPR1 = OUTPUT OF MOLECULAR TRANSMITTANCE
DATA MAXGEO / 68/
small = 2.0
IP4 = 14
IRD = 5
IPR = 6
IP6 = 16
IP6S= 26
IPU = 7
IP7 = 17
IPR1= 8
IP8 = 18
IRDS = 29
ITR = 30
ISCRCH = 10
ITM = 31
Isky = 32
Isun = 33
Ipath = 34
OPEN (IRD, FILE='TAPE5', STATUS='OLD') driv 720
OPEN (IPR, FILE='TAPE6', STATUS='UNKNOWN') driv 730
OPEN (IP6, FILE='OUT', STATUS='UNKNOWN') driv 740
OPEN (IPU, FILE='TAPE7', STATUS='UNKNOWN')
OPEN (IP7, FILE='TAPE7.PLT', STATUS='UNKNOWN') driv 750
OPEN (IPR1,FILE='TAPE8', STATUS='UNKNOWN')
OPEN (IP8, FILE='TAPE8.PLT', STATUS='UNKNOWN')
OPEN (IP4, FILE='OUT.PLT', STATUS='UNKNOWN')
OPEN (ITR, FILE='TRANS.PLT', STATUS='UNKNOWN')
OPEN (ISCRCH,STATUS='SCRATCH', FORM='UNFORMATTED') driv 760
OPEN (Isky, FILE='Sky.plt', STATUS='UNKNOWN')
OPEN (Isun, FILE='Sun.plt', STATUS='UNKNOWN')
OPEN (Ipath,FILE='Path.plt',STATUS='UNKNOWN')
OPEN (ITM, FILE='TIME', STATUS='UNKNOWN')

C
C ALTITUDE PARAMETERS
C
C ZMDL COMMON/MODEL/ THE ALTITUDES USED IN LOWTRAN
C ZCVSA,ZTVSA,ZIVSA CARD 3.3 LOWTRAN FOR VSA INPUT
C ZVSA NINE ALTITUDES GEN BY VSA ROUTINE
C
Pix=2.0*ASIN(1.0) driv 770
CA=Pix/180. driv 780

```

```

DEG= 1.0/CA          driv 860
pi      = Pix
r2d     = 180./pi
d2r     = pi/180.
epsilon = d2r*0.2659
delta   = 1.4E-6
onem   = 1. - delta
onep   = 1. + delta
infinity = 999999
RANGE=0.0           driv 870
C*****GCAIR IS THE GAS CONSTANT FOR AIR IN UNITS OF MB/(GM CM-3 K) driv 880
GCAIR = 2.87053E+3  driv 890
C*****BIGNUM AND BIGEXP ARE THE LARGEST NUMBER AND THE LARGEST ARGUMENT driv 900
C*****EXP ALLOWED AND ARE MACHINE DEPENDENT. THE NUMBERS USED HERE ARE Fdrv 910
C*****A TYPICAL 32 BIT-WORD COMPUTER. driv 920
    BIGNUM = 1.0E35          driv 930
    BIGEXP = 87.0            driv 940
C      THE VALUES FOR BIGNUM AND BIGEXP FOLLOW THE          driv 950
C      DESCRIPTION UNDER EXP FUNCTION IN "IBM SYSTEM 360/          driv 960
C      AND SYSTEM 370 FORTRAN IV LANGUAGE"          driv 970
C      BIGNUM = 4.3E68          driv 980
C      BIGEXP = 174.6          driv 990
KMAX=63             driv1000
C*****NL IS THE NUMBER OF BOUNDARIES IN THE STANDARD MODELS 1 TO 6 driv1010
C*****BOUNDARY 34 (AT 99999 KM) IS NO LONGER USED          driv1020
    NL = 33             driv1030
*****
Sea    = .FALSE.
SeaOld = .FALSE.
Hit   = .FALSE.
Msea  = -1
Done   = .FALSE.
*****
C*****CALL TIME AND DATE:          driv1040
C*****THE USER MAY WISH TO INCLUDE SUBROUTINES FDATE AND FCLOCK WHICH driv1050
C*****RETURN THE DATE AND TIME IN MM/DD/YY AND HH.MM.SS FORMATS driv1060
C*****RESPECTIVELY. THE REQUIRED ROUTINES FOR A CDC 6600 ARE INCLUDED ATdrv1070
C*****THE MAIN PROGRAM IN COMMENT CARDS. driv1080
C@    CALL FDATE(HDATE)          driv1090
C@    CALL FCLOCK(HTIME)          driv1100
    CALL DATE (Date$)
    CALL TIME (Time$)
C
C*****START CALCULATION          driv1110
C
C
100   DO 10 II = 1,4          driv1120
10    IREG(II) = 0            driv1130
    WRITE(IPR,1000)          driv1140
1000  FORMAT('1',20X,'***** MODTRAN *****')
C@    WRITE(IPR,1010) HDATE,HTIME          driv1150
1010  FORMAT('1',20X,'***** MODTRAN *****',10X,2(1X,A8,1X))          driv1160
    DO 80 I=1,4
        DO 80 J=1,40          driv1170
            ABSC(I,J)=0.
            EXTC(I,J)=0.
80    ASYM(I,J)=0.          driv1180
                                driv1190
                                driv1200
                                driv1210
                                driv1220
                                driv1230
                                driv1240
                                driv1250

```

```

JPRT = 0                                driv1260
IKLO=1                                  driv1270
C                                         driv1280
C*****CARD 1                            driv1290
C                                         driv1300
C
READ(IRD,'(L1,I4,12I5,F8.3,F7.2)')MODTRN,MODEL,ITYPE,
+          IEMSCT,IMULT,M1,M2,M3,M4,M5,M6,MDEF,IM,NOPRT,TBOUND,SALB driv1340
1110 FORMAT(13I5,F8.3,F7.2)                driv1350
***** Save parameters to restore them
ITYPEold = ITYPE
IEMSCTold = IEMSCT
IMULTold = IMULT
If (TBOUND .EQ. 0.) TBOUND = 0.1
TBOUNDold = TBOUND
SALBold = SALB
***** in case new geometry cards are
C                                     later introduced via file TAPE5.SEA
IF (MODTRN) THEN
    Prog$ = 'MODTRAN2 *****'
ELSE
    Prog$ = 'LOWTRAN7 *****'
END IF
WRITE (IP6, 1018) Prog$
1018 FORMAT(15X, '***** SEARAD, A MODIFICATION OF ', A14)
WRITE (IP6, 1020) Date$, Time$
1020 FORMAT (/, 'DATE:', 1X, A8, T60, 'TIME:', 1X, A8)
SELECT CASE (IEMSCT)
    CASE (0)
        WRITE (IP6, '(/, 18HTRANSMITTANCE MODE)')
    CASE (1)
        WRITE (IP6, '(/, 21HTHERMAL RADIANCE MODE)')
    CASE (2)
        WRITE (IP6, '(/, 32HTHERMAL PLUS SOLAR RADIANCE MODE)')
    CASE (3)
        WRITE (IP6, '(/, 21HSOLAR IRRADIANCE MODE)')
END SELECT
C
SELECT CASE (IMULT)
    CASE (0)
        PRINT *, "IMULT = ", IMULT, ": BEWARE OF BEN-SHALOM"
        WRITE (IP6, '(/, 22HSINGLE SCATTERING USED)')
    CASE (1)
        WRITE (IP6, '(/, 24HMULTIPLE SCATTERING USED)')
END SELECT
C
WRITE(IPR,'(15H0 CARD 1 *****,L1,I4,12I5,F8.3,F7.2)')MODTRN,MODELdriv1380
1 ,ITYPE,IEMSCT,IMULT,M1,M2,M3,M4,M5,M6,MDEF,IM,NOPRT,TBOUND,SALB driv1390
1111 FORMAT('0 CARD 1 *****',13I5,F8.3,F7.2)                      driv1400
C IF(IMULT .EQ. 1 .AND. NOPRT.EQ. 1) NOPRT = 0                      driv1410
C                                         driv1420
C SET THE NUMBER OF SPECIES TREATED WITH THE 1 CM-1 BAND MODEL. driv1430
C ALSO, FOR EACH SPECIES, SET THE POINTER WHICH MAPS THE HITRAN driv1440
C NUMERICAL LABEL TO THE LOWTRAN NUMERICAL LABEL.                     driv1450
C                                         driv1460
NSPEC=12                           driv1470
KPOINT( 1)=17                         driv1480
KPOINT( 2)=36                         driv1490

```

```

KPOINT( 3)=31                         driv1500
KPOINT( 4)=47                         driv1510
KPOINT( 5)=44                         driv1520
KPOINT( 6)=46                         driv1530
KPOINT( 7)=50                         driv1540
KPOINT( 8)=54                         driv1550
KPOINT( 9)=56                         driv1560
KPOINT(10)=55                         driv1570
KPOINT(11)=52                         driv1580
KPOINT(12)=11                         driv1590
C
IRD1 = 0                             driv1600
IRD2 = 0                             driv1610
IF (MODEL.EQ.0) LEN = 0               driv1620
IF((MODEL.EQ.0) .OR. (MODEL.EQ.7)) GO TO 110
IF(M1.EQ.0) M1=MODEL                 driv1630
IF(M2.EQ.0) M2=MODEL                 driv1640
IF(M3.EQ.0) M3=MODEL                 driv1650
IF(M4.EQ.0) M4=MODEL                 driv1660
IF(M5.EQ.0) M5=MODEL                 driv1670
IF(M6.EQ.0) M6=MODEL                 driv1680
IF(MDEF.EQ.0) MDEF=1                 driv1690
110  CONTINUE
M=MODEL
NPR = NOPRT
C*****CARD 2 AEROSOL MODEL
READ(IRD,1200)IHAZE,ISEASN,IVULCN,ICSTL,ICLD,IVSA,VIS,WSS,WHH,
1 RAINRT,GNDALT                     driv1700
1200  FORMAT(6I5,5F10.3)
      WRITE(IPR,1201)IHAZE,ISEASN,IVULCN,ICSTL,ICLD,IVSA,VIS,WSS,WHH,
1 RAINRT,GNDALT                     driv1710
      IF(GNDALT.GT.0.) WRITE(IPR,1199)GNDALT
1199  FORMAT(1H0,' GNDALT =',F10.2)
      IF(GNDALT.GE.6.0) THEN
          WRITE(IPR,1202)GNDALT
          GNDALT=0.
      ENDIF
1201  FORMAT('0 CARD 2 *****',6I5,5F10.3)
1202  FORMAT('0 GNDALT GT 6.0 RESET TO ZERO, GNDALT WAS',F10.3)
C
      IF(VIS.LE.0.0.AND.IHAZE.GT.0) VIS=VSB(IHAZE)
      RHH= 0.
      IF(MODEL.EQ.0.OR.MODEL.EQ.7) GO TO 205
      IF((MODEL.EQ.3.OR.MODEL.EQ.5).AND.ISEASN.EQ.0) ISEASN=2
C
      IF(IVSA.EQ.1 .AND. IHAZE.EQ.3)           driv1940
1 CALL MARINE(VIS,MODEL,WSS,WHH,ICSTL,EXTC,ABSC,1)   driv1950
      ICH(1)=IHAZE                           driv1960
      ICH(2)=6                               driv1970
      ICH(3)=9+IVULCN                      driv1980
205  IF(RAINRT.EQ.0) GO TO 210             driv1990
      WRITE(IPR,1205) RAINRT                driv2000
1205  FORMAT('0 RAIN MODEL CALLED, RAIN RATE = ',F9.2,' MM/HR')  driv2010
210  ICH(4)=18                            driv2020
      IF(ICL(1).LE.0) ICH(1)=1              driv2030
      IF(ICL(3).LE.9) ICH(3)=10            driv2040
      IF(ICLD.GE.1 .AND. ICLD.LE.11) THEN  driv2050
                                         driv2060

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      ICH(4)=ICH(3)          driv2070
      ICH(3)=ICH(2)          driv2080
      ICH(2)=ICLD            driv2090
END IF                         driv2100
IFLGA=0                         driv2110
IFLGT=0                         driv2120
CTHIK=-99.                      driv2130
CALT=-99.                       driv2140
CEXT=-99.                       driv2150
ISEED=-99                        driv2160
IF(ICLD .LT. 18) GO TO 230      driv2170
C*****CARD 2A CIRRUS CLOUDS    driv2180
READ(IRD,1210)CTHIK,CALT,CEXT,ISEED   driv2190
1210 FORMAT(3F10.3,I10)           driv2200
WRITE(IPR,1211)CTHIK,CALT,CEXT,ISEED   driv2210
1211 FORMAT('0 CARD 2A *****',3F10.3,I10)  driv2220
230 CONTINUE                      driv2230
C*****CARD 2B VERTICAL STRUCTURE ALGORITHM
ZCVSA=-99.                      driv2240
ZTVSA=-99.                       driv2250
ZINVSA=-99.                      driv2260
ZINVSA=-99.                      driv2270
C
      IF( IVSA. EQ. 0 ) GO TO 240   driv2280
      READ (IRD,1230) ZCVSA,ZTVSA,ZINVSA   driv2290
1230 FORMAT(3F10.3)           driv2300
      WRITE(IPR,1231) ZCVSA,ZTVSA,ZINVSA   driv2310
1231 FORMAT('0 CARD 2B *****',3F10.3)  driv2320
C
      CALL VSA(IHAZE,VIS,ZCVSA,ZTVSA,ZINVSA,ZVSA,RHVSA,AHVSA,IHVSA)  driv2330
C
      END OF VSA MODEL SET-UP      driv2340
C
240  IF (MODEL.NE.0 .AND. MODEL.NE.7 ) ML=NL   driv2350
      MDELS=MODEL                 driv2360
      DO 250 I=1,5                driv2370
          IF(MDELS.NE.0)HMODEL(I,7)=HMODEL(I,MDELS)  driv2380
250  IF(MDELS.EQ.0)HMODEL(I,7)=HMODEL(I,8)   driv2390
C
      IF(IM .EQ. 1) THEN          driv2400
          IF((MODEL.EQ.7.AND.IM.EQ.1) .OR.(MODEL.EQ.0)) THEN  driv2410
C
C*****CARD 2C USER SUPPLIED ATMOSPHERIC PROFILE
C
      READ (IRD,1250) ML,IRD1,IRD2,(HMODEL(I,7),I=1,5)  driv2420
1250 FORMAT(3I5,18A4)           driv2430
      WRITE(IPR,1251)ML,IRD1,IRD2,(HMODEL(I,7),I=1,5)  driv2440
          IF(IVSA.EQ.1)CALL RDNSM   driv2450
1251 FORMAT('0 CARD 2C *****',3I5,18A4)  driv2460
      ENDIF                      driv2470
ENDIF                         driv2480
M=7                           driv2490
CALL AERNSM(JPRT, GNDALT)     driv2500
IF(ICLD .LT. 20) GO TO 260    driv2510
C
C
      SET UP CIRRUS MODEL        driv2520
C
      IF(CTHIK.NE.0) IFLGT=1     driv2530

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IF(CALT.NE.0) IFLGA=1 driv2640
IF(ISEED.EQ.0) IFLGT=2 driv2650
IF(ISEED.EQ.0) IFLGA=2 driv2660
CALL CIRRUS(CTHIK,CALT,ISEED,CPROB,CEXT) driv2670
WRITE(IPR,1220) driv2680
1220 FORMAT(15X,'CIRRUS ATTENUATION INCLUDED (N O A A CIRRUS) ') driv2690
IF(IFLGT.EQ.0) WRITE(IPR,1221) CTHIK driv2700
1221 FORMAT(15X,'CIRRUS ATTENUATION STATISTICALLY DETERMINED TO BE', driv2710
1 F10.3,'KM') driv2720
IF(IFLGT.EQ.1) WRITE(IPR,1222) CTHIK driv2730
1222 FORMAT(15X,'CIRRUS THICKNESS USER DETERMINED TO BE',F10.3,'KM') driv2740
IF(IFLGT.EQ.2) WRITE(IPR,1223) CTHIK driv2750
1223 FORMAT(15X,'CIRRUS THICKNESS DEFAULTED TO MEAN VALUE OF ', driv2760
1 F10.3,'KM') driv2770
IF(IFLGA.EQ.0) WRITE(IPR,1224) CALT driv2780
1224 FORMAT(15X,'CIRRUS BASE ALTITUDE STATISTICALLY DETERMINED TO BE', driv2790
1 F10.3,' KM') driv2800
IF(IFLGA.EQ.1) WRITE(IPR,1225) CALT driv2810
1225 FORMAT(15X,'CIRRUS BASE ALTITUDE USER DETERMINED TO BE', driv2820
1 F10.3,' KM') driv2830
IF(IFLGA.EQ.2) WRITE(IPR,1226) CALT driv2840
1226 FORMAT(15X,'CIRRUS BASE ALTITUDE DEFAULTED TO MEAN VALUE OF ', driv2850
1 F10.3,'KM') driv2860
WRITE(IPR,1227) CPROB driv2870
1227 FORMAT(15X,'PROBABILITY OF CLOUD OCCURRING IS',F7.1,' PERCENT') driv2880
C driv2890
C END OF CIRRUS MODEL SET UP driv2900
C driv2910
260 CONTINUE driv2920
C driv2930
C driv2940
C*****CARD 2E driv2950
C driv2960
IF((IHAZE.EQ.7).OR.(ICLD.EQ.11)) THEN driv2970
C driv2980
C***** CARD 2E USER SUPPLIED AEROSOL EXTINCTION, ABSORPTION, AND driv2990
C ASYMMETRY driv3000
CALL RDEXA driv3010
C driv3020
ENDIF driv3030
300 CONTINUE driv3040
driv3050
IPARM ==-99 driv3060
IPH ==-99 driv3070
IDAY ==-99 driv3080
ISOURC==-99 driv3090
C driv3100
PARM1 ==-99. driv3110
PARM2 ==-99. driv3120
PARM3 ==-99. driv3130
PARM4 ==-99. driv3140
GMT ==-99. driv3170
PSIPO = 0. driv3180
ANGLEM=-99. driv3190
G ==-99. driv3200
C
C*****CARD 3 GEOMETRY PARAMETERS

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C                                         driv3210
C     IF ((SEA) .AND. (Msea .EQ. 0)) THEN
C         the first sky card is next.
C         Set emissivity to zero (TBOUND is already zero) and ITYPE to 3
C         for calculations coming up with cards in TAPE5.SEA:
C             ITYPE = 3
C             SALB = 0.0
C         END IF
*** Set mode to sun irradiance (if a sun card will be next) *****
C     IF ((Sea) .AND. (IEMSCTold .EQ. 2) .AND. (Msea .EQ. 3)) THEN
C         IEMSCT = 3
C         IMULT = 0
C         LFIRST = .TRUE.
C         LSAME = .FALSE.
C     END IF
C     IF (IEMSCT .EQ. 3) GO TO 315                                         driv3220
***** Read introduced geometry cards from file TAPE5.SEA *****
C     IF (SEA) THEN
C         READ(IRDS,1312)H1,H2,ANGLE,RANGE,BETA,RO,LEN,Psi,SeaSwitch
C     ELSE
C         READ (IRD,1312)H1,H2,ANGLE,RANGE,BETA,RO,LEN,Psi,SeaSwitch
C     END IF
***** and remove the boundary (in sea AND sky) for a sea calculation ***
C     IF (SeaSwitch) TBOUND = 0.1
1312 FORMAT(6F10.3,I5,F10.3,L5)                                         driv3240
C     WRITE(IPR,1313)H1,H2,ANGLE,RANGE,BETA,RO,LEN,Psi,SeaSwitch
1313 FORMAT('0 CARD 3 *****',6F10.3,I5,F10.3,L5)                         driv3260
C     GO TO 320                                                       driv3270
C
C*****CARD 3 FOR DIRECTLY TRANSMITTED SOLAR RADIANCE (IEMSCT = 3)          driv3280
C
C     315 CONTINUE                                                 driv3290
***** Read introduced sun card from file TAPE5.SEA *****
C     IF (Sea) THEN
C         READ(IRDS,1316) H1,H2,ANGLE,IDAY,RO,ISOURC,ANGLEM
C     ELSE
C         READ(IRD, 1316) H1,H2,ANGLE,IDAY,RO,ISOURC,ANGLEM           driv3300
C     END IF
*****
1316 FORMAT(3F10.3,I5,5X,F10.3,I5,F10.3)                                driv3310
C     WRITE(IPR,1317) H1,H2,ANGLE,IDAY,RO,ISOURC,ANGLEM                 driv3320
1317 FORMAT('0 CARD 3 *****',3F10.3,I5,5X,F10.3,I5,F10.3)            driv3330
C     ITYPE = 3
C     RANGE = 0.0
C     BETA = 0.0
C     LEN = 0
C*****RO IS THE RADIUS OF THE EARTH
320  RE=6371.23
C     ***** ERRATA JULY 25
C         IF(H1. LT. ZM(1) ) THEN
C             WRITE(IPR,905) H1,ZM(1)
905   X     FORMAT(' H1 LESS THAN FIRST ALT RESET ',/
C             ' H1 WAS ',F10.2,' 1ST ALT = ',F10.2)
C             H1 = ZM(1)
C         ENDIF
C     ***** END ERRATA
C     H1S = H1

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H2S      = H2          driv3490
ANGLES   = ANGLE       driv3500
RANGS   = RANGE        driv3510
BETAS    = BETA         driv3520
ITYPES   = ITYPE        driv3530
LENS     = LEN          driv3540
IF (MODEL.EQ.0) RO = RE  driv3560
IF (MODEL.EQ.1) RE=6378.39 driv3570
IF (MODEL.EQ.4) RE=6356.91 driv3580
IF (MODEL.EQ.5) RE=6356.91 driv3590
IF (RO.GT.0.0) RE=RO     driv3600
C
C      IF (IEMSCT.NE.2) GO TO 330  driv3610
C
C*****CARD 3A1           driv3620
C
C      IF (SEA) THEN
C          READ(IRDS,1320) IPARM,IPH,IDAY,ISOURC
C          ELSE
C              READ(IRD,1320) IPARM,IPH,IDAY,ISOURC
C          END IF
1320  FORMAT(4I5)
C          WRITE(IPR,1321) IPARM,IPH,IDAY,ISOURC
1321  FORMAT('0 CARD 3A1*****',4I5)
C
C*****CARD 3A2           driv3700
C
C      IF (SEA) THEN
C          READ(IRDS,1322) PARM1, PARM2, PARM3, PARM4,
C          +                 GMT,PSIPO,ANGLEM,G
C          ELSE
C              READ(IRD,1322) PARM1, PARM2, PARM3, PARM4,
C          +                 GMT,PSIPO,ANGLEM,G
C          END IF
1322  FORMAT(8F10.3)
C          WRITE(IPR,1323) PARM1, PARM2, PARM3, PARM4,GMT,PSIPO,ANGLEM,G
1323  FORMAT('0 CARD 3A2*****',8F10.3)
C
CSSISSISSISSISSI CHANGES BEGIN.
C
C      REWIND(ISCRCH)          driv3780
C
C      IF (LFIRST .AND. IMULT .EQ. 1) THEN  driv3790
C
C          SAVE SOLAR PARAMETERS FOR COMPARING LATER.  driv3800
C          NOTE THAT LFIRST IS TRUE AND IMULT (MULTIPLE SOLAR SCATTERING)  driv3810
C          LFIRST = .FALSE.          driv3820
C          CALL SVSOLA(IPARM,IPH,IDAY,ISOURC,PARM1,PARM2,PARM3,PARM4,  driv3830
C          +                 GMT,PSIPO,ANGLEM,  driv3840
C          +                 ISAVE1,ISAVE2,ISAVE3,ISAVE4,SAVE1,SAVE2,SAVE3,SAVE4,  driv3850
C          +                 SAVE5,SAVE6,SAVE7)          driv3860
C          LSAME = .FALSE.          driv3870
C
C      ELSEIF (IMULT .EQ. 1 .AND. IRPT .EQ. 3) THEN  driv3890
C
C          NOW COMPARE SOLAR PARAMETERS; LSAME IS TRUE IF THEY MATCH.  driv3900
C          CALL COMPAR(IPARM,IPH,IDAY,ISOURC,PARM1,PARM2,PARM3,PARM4,  driv3910
C
C

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$      GMT,PSIPO,ANGLEM,
$      ISAVE1,ISAVE2,ISAVE3,ISAVE4,SAVE1,SAVE2,SAVE3,SAVE4,      driv3980
$      SAVE5,SAVE6,SAVE7,LSAME)                                driv3990
$      CALL SVSOLA(IPARM,IPH,IDAY,ISOURC,PARM1,PARM2,PARM3,PARM4,  driv4000
$      GMT,PSIPO,ANGLEM,
$      ISAVE1,ISAVE2,ISAVE3,ISAVE4,SAVE1,SAVE2,SAVE3,SAVE4,      driv4020
$      SAVE5,SAVE6,SAVE7)                                driv4030
$      ELSE                                              driv4040
C
C      GET READY FOR ANOTHER POSSIBLE FORTHCOMING SERIES OF MULTIPLE  driv4050
C      SOLAR SCATTERING RUNS.                                driv4060
LFIRST = .TRUE.                                         driv4070
LSAME = .FALSE.                                         driv4080
ENDIF                                              driv4090
C
CSSISSISSISSISSI CHANGES END                         driv4100
C
IF(IPH.EQ.0) THEN                                     driv4110
  IF(G.GE.1.0) G = .9999                            driv4120
  IF(G.LE.-1.0) G = -.9999                           driv4130
ENDIF                                              driv4140
IF(IPH.NE.1) GO TO 330                             driv4150
C
C*****CARD 3B1 USER DEFINED PHASE FUNCTION          driv4160
C
C*****READ USER DEFINED PHASE FUNCTION             driv4170
C
READ(IRD,1326)NANGLS                               driv4180
1326 FORMAT(I5)                                    driv4190
WRITE(IPR,1327)NANGLS                            driv4200
1327 FORMAT(' CARD 3B1*****',I5)                  driv4210
C
C*****CARD 3B2
C
READ(IRD,1328)(ANGF(I),F(1,I),F(2,I),F(3,I),F(4,I),I=1,NANGLS)  driv4220
1328 FORMAT(5E10.3)                                driv4230
WRITE(IPR,1329)(ANGF(I),F(1,I),F(2,I),F(3,I),F(4,I),I=1,NANGLS)  driv4240
1329 FORMAT('0 CARD 3B2*****',5E10.3)              driv4250
C
330 CONTINUE                                         driv4260
C
IF(IRPT.EQ.3) THEN                                 driv4270
  IF(IPARM.EQ.1) CALL SUBSOL(PARM3,PARM4,GMT,IDAD)  driv4280
  GO TO 555                                         driv4290
END IF                                              driv4300
C
C*****CARD 4 WAVENUMBER                           driv4310
C
400 CONTINUE                                         driv4320
IF(.NOT.SEA) THEN
  READ(IRD,'(5I10)')IV1,IV2,IDV,IFWHM,IFILTER
END IF
401 WRITE(IPR,'(15H0 CARD 4 *****,5I10)')IV1,IV2,IDV,IFWHM,IFILTER
IF(IDV.LE.0)THEN
  PRINT *, ' ERROR IN IDV ',IDV
  IDV = 1
ENDIF

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IF(IFWHM . LE. 0)THEN driv4570
  PRINT *, ' ERROR IN IFWHM ',IFWHM
  IFWHM = 2 driv4580
ENDIF driv4590
IF ((IFILTER .GE. 1) .AND. (IFILTER .LE. 6)) THEN driv4600
C      reset wavenumbers to span filter passband:
  W1 = FLIST(1, IFILTER)
  W2 = FLIST(2, IFILTER)
  IV1 = INT(1E4/W2) - IDV
  IV2 = INT(1E4/W1) + IDV
ELSE
  filter data are absent. Reset to no filter at all:
  IFILTER = 0
END IF
IF (SeaSwitch) THEN
  Check number of wavenumber steps. Reset, if necessary, to
  prevent sea arrays from overflowing in "TRANS".
  Nv = (IV2 - IV1)/IDV
  IF (Nv .GE. Kv) IDV = (IV2 - IV1)/Kv + 1
END IF
WRITE(IP4, '(1H\, T20, 22HOUTPUT FILE FOR FILTER, I2,
+           2H: , I5, 3H TO, I5, 9H CM-1 IN , I2,
+           12H CM-1 STEPS., /1H\)' ) IFILTER, IV1, IV2, IDV
WRITE(IP4, '(1H\, T65, 18H FILTERED RADIANCE)')
WRITE(IP4, '(45H\          ELEV.    ANGLE RANGE     TRANS ,
+           T49, 34H PATH      SEA      SKY      SUN,
+           T88, 15H TOTAL    TEMP.)')
WRITE(IP4, '(45H\          (mrad)   (deg)   (km)   (--) ,
+           T68,13H (W m-2 sr-1), T100, 3H(C), /)')
IF(IHAZE.EQ.3) THEN driv4610
C      IF(V1.LT.250.0 .OR. V2.LT.250.0) THEN driv4620
  IF(IV1.LT.250) THEN driv4630
    IHAZE=4 driv4640
    WRITE (IPR,1203) driv4650
  ENDIF driv4660
1203  FORMAT('0**WARNING** NAVY MODEL IS NOT USABLE BELOW 250CM-1', driv4670
1      //,10X,' PROGRAM WILL SWITCH TO IHAZE=4 LOWTRAN 5 MARITIME',//)driv4680
END IF driv4690
IF (IRPT.EQ.4) GO TO 550 driv4700
cc  IF (IRPT.EQ.-4) GO TO 560 driv4710
500  CONTINUE driv4720
IF (IRPT.EQ.3) GO TO 555 driv4730
WRITE(IPR,1410) (HTRRAD(I1,IEMSCT+1),I1=1,6) driv4740
1410  FORMAT('0 PROGRAM WILL COMPUTE ',6A4) driv4750
IF(ISOURC .EQ. 1) WRITE(IPR,1204) driv4760
1204  FORMAT(' LUNAR SOURCE ONLY ') driv4770
IF (IMULT .EQ. 1) THEN driv4780
  IF(IEMSCT.EQ.0 .OR. IEMSCT.EQ.3 ) THEN
    WRITE(IPR,1411) driv4790
  FORMAT('0 MULTIPLE SCATTERING HAS BEEN TURNED OFF ') driv4800
1411  WRITE (IP6,
+           '(/, 39HMULTIPLE SCATTERING HAS BEEN TURNED OFF') ) driv4810
  IMULT=0 driv4820
ELSE driv4830
  WRITE(IPR,1412) driv4840
END IF driv4850
END IF driv4860

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1412 FORMAT('0 CALCULATIONS WILL BE DONE USING MULTIPLE SCATTERING ') driv4870
MDEL=MODEL driv4880
IF(MDEL.EQ.0)MDEL=8 driv4890
MM1=MDEL driv4900
MM2=MDEL driv4910
MM3=MDEL driv4920
IF(M1.NE.0)MM1=M1 driv4930
IF(M2.NE.0)MM2=M2 driv4940
IF(M3.NE.0)MM3=M3 driv4950
IF(MODEL.EQ.0) GO TO 510 driv4960
WRITE(IPR,1500) MM1,(HMODEL(I1,MM1),I1=1,5),MM2,(HMODEL(I2,MM2),
1 I2=1,5),MM3,(HMODEL(I3,MM3),I3=1,5) driv4970
1500 FORMAT('0 ATMOSPHERIC MODEL',//,
1 10X,'TEMPERATURE = ',I4,5X,5A4,//,
1 10X,'WATER VAPOR = ',I4,5X,5A4,//,
1 10X,'OZONE = ',I4,5X,5A4) driv4980
WRITE(IPR,1501) M4,M5,M6,MDEF driv4990
1501 FORMAT(20X,' M4 = ',I5,' M5 = ',I5,' M6 = ',I5,' MDEF = ',I5) driv5000
C driv5010
510 IF(JPRT.EQ.0) GO TO 520 driv5020
IF(ISEASN.EQ.0)ISEASN=1 driv5030
IF(IVULCN.LE.0) IVULCN=1 driv5040
IHVUL=IVULCN+10 driv5050
IF( IVULCN .EQ. 6) IHVUL = 11 driv5060
IF( IVULCN .EQ. 7) IHVUL = 11 driv5070
IF( IVULCN .EQ. 8) IHVUL = 13 driv5080
IHMET=1 driv5090
IF(IVULCN.GT.1)IHMET=2 driv5100
IF(IHAZE.EQ.0) GO TO 520 driv5110
WRITE(IPR,1510)(HHAZE(I,IHAZE),I=1,5),VIS,(HHAZE(I2,6),I2=1,5),
1 (HHAZE(II,6),II=1,5),(HSEASN(IA,ISEASN),IA=1,5), driv5120
2 (HHAZE(I3,IHVUL),I3=1,5), driv5130
3 (HVULCN(IB,IVULCN),IB=1,5),(HSEASN(IC,ISEASN),IC=1,5), driv5140
4 (HHAZE(I4,16),I4=1,5),(HMET(I5,IHMET),I5=1,5) driv5150
1510 FORMAT('0 AEROSOL MODEL',//,10X,'REGIME',
A T35,'AEROSOL TYPE',T60,'PROFILE',T85,'SEASON',//,/,
B 10X,'BOUNDARY LAYER (0-2 KM)',T35,5A4,T60,F5.1, driv5160
C ' KM VIS AT SEA LEVEL',//,10X,'TROPOSPHERE (2-10KM)',T35, driv5170
D 5A4,T60,5A4,T85,5A4,//,10X,'STRATOSPHERE (10-30KM)', driv5180
E T35,5A4,T60,5A4,T85,5A4,//,10X,'UPPER ATMOS (30-100KM)', driv5190
F T35,5A4,T60,5A4) driv5200
520 CONTINUE driv5210
IF(ITYPE.EQ.1) THEN
    WRITE(IPR,1515) H1,RANGE driv5220
    WRITE(IP6,1515) H1,RANGE
END IF driv5230
1515 FORMAT(//,' HORIZONTAL PATH',//,
1 8X,'ALTITUDE = ',F10.3,' KM',//,
2 8X,'RANGE = ',F10.3,' KM',//) driv5240
IF(ITYPE.EQ.2) THEN
    WRITE(IPR,1516) H1,H2,ANGLE,RANGE,BETA,LEN driv5250
    WRITE(IP6,1516) H1,H2,ANGLE,RANGE,BETA,LEN
END IF driv5260
1516 FORMAT(//,' SLANT PATH, H1 TO H2',//,
1 10X,'H1 = ',F10.3,' KM',//,10X,'H2 = ',F10.3,' KM',//, driv5270
2 10X,'ANGLE = ',F10.3,' DEG',//,10X,'RANGE = ',F10.3,' KM',//, driv5280
3 10X,'BETA = ',F10.3,' DEG',//,10X,'LEN = ',I6,/) driv5290

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        IF(ITYPE.EQ.3) THEN
          WRITE(IPR,1517) H1,H2,ANGLE
          WRITE(IP6,1517) H1,H2,ANGLE
        END IF
1517  FORMAT(//,'SLANT PATH TO SPACE',//,
1      10X,'H1      = ',F10.3,' KM',//,
2      10X,'HMIN    = ',F10.3,' KM',//,
3      10X,'ANGLE   = ',F10.3,' DEG',//)
      IF (IEMSCT.NE.2) GO TO 550
C
C*****INTREPRET SOLAR SCATTERING PARAMETERS
C
C
      IF (IPARM.EQ.1) CALL SUBSOL (PARM3,PARM4,GMT,IDAY)
C
      WRITE (IPR,1530)
1530  FORMAT('0 SINGLE SCATTERING CONTROL PARAMETERS SUMMARY ')
      IF(IPARM.NE.2) WRITE (IPR,1532) PARM1,PARM2,PARM3,PARM4,GMT,PSIPO
      1, IDAY
1532  FORMAT(10X,'OBSERVER LATITUDE =',T35,F10.2,' DEG NORTH OF EQUATOR'drv5520
      1 ,/,10X,'OBSERVER LONGITUDE=',T35,F10.2,' DEG WEST OF GREENWICH',drv5530
      2 ,/,10X,'SUBSOLAR LATITUDE =',T35,F10.2,' NORTH OF EQUATOR',//,     driv5540
      3 10X,'SUBSOLAR LONGITUDE =',T35,F10.2,' WEST OF GREENWICH',//,     driv5550
      4 10X,'TIME (<0 IS UNDEF)=',T35,F10.3,' GREENWICH TIME',//,     driv5560
      5 10X,'PATH AZIMUTH =',T35,F10.3,' DEG EAST OF NORTH',//,     driv5570
      6 10X,'DAY OF YEAR =',T35,I10)                                     driv5580
      IF (IPARM.EQ.2) WRITE (IPR,1534) PARM1,PARM2,GMT,PSIPO, IDAY
1534  FORMAT(10X,'RELATIVE AZIMUTH =',T35,F10.3,' DEG EAST OF NORTH',//, driv5600
      1 10X,'SOLAR ZENITH =',T35,F10.3,' DEG ',/,                         driv5610
      2 10X,'TIME (<0 UNDEF) =',T35,F10.3,' GREENWICH TIME',//,           driv5620
      3 10X,'PATH AZIMUTH =',T35,F10.3,' DEG EAST OF NORTH',//,           driv5630
      4 10X,'DAY OF THE YEAR =',T35,I16)                                 driv5640
      IF (ISOURC.EQ.0) WRITE (IPR,1535)
1535  FORMAT('0 EXTRATERRESTRIAL SOURCE IS THE SUN')                   driv5660
      IF (ISOURC.EQ.1) WRITE (IPR,1536) ANGLEM
1536  FORMAT('0 EXTRATERRESTRIAL SOURCE IS THE MOON, MOON PHASE ANGLE =',drv5680
      1 F10.2,' DEG')
      IF (IPH.EQ.0) WRITE (IPR,1538) G
1538  FORMAT('0 H-G PHASE FUNCTION ,G=',F10.3)                         driv5710
      IF (IPH.EQ.1) WRITE (IPR,1540)
1540  FORMAT('0 USER SUPPLIED PHASE FUNCTION')                         driv5730
      IF (IPH.EQ.2) WRITE (IPR,1542)
1542  FORMAT('0 PHASE FUNCTION FROM MIE DATA BASE')                   driv5750
550   CONTINUE
C      V1 =FLOAT(INT(V1/5.0+0.1))*5.0                                driv5770
C      V2 =FLOAT(INT(V2/5.0+0.1))*5.0                                driv5780
C      TO AVOID THE DIFFICULTY FOR V1=0
      ALAM1= 99999.98                                                 driv5790
C      IF(V1.GT.0.)ALAM1=10000./V1                                    driv5810
C      ALAM2=10000./V2
C      IF(DV.LT.5.)DV=5.
C      DV=FLOAT(INT(DV/5+0.1))*5.0                                driv5840
C      WRITE (IPR,1555) V1,ALAM1,V2,ALAM2,DV
C1555  FORMAT('0 FREQUENCY RANGE ',10X,' V1 = ',F12.1,' CM-1 (',
C      1 F10.2,' MICROMETERS',//,10X,' V2 = ',F12.1,' CM-1 (',F10.2,
C      2 ' MICROMETERS',//,10X,' DV = ',F12.1,' CM-1')             driv5860
      IF(.NOT.MODTRN)THEN                                            driv5870
                                                driv5880
                                                driv5890

```

```

        IV1=5*(IV1/5)
        IV2=5*((IV2+4)/5)
        IDV=5+5*((IDV-5)/5)
    ENDIF
    IF(IV2.LT.IV1+IDV)THEN
        WRITE(IPR,'(/41H IV2 WAS LESS THAN IV1 + IDV AND HAS BEEN,
1           6H RESET,/)')
        IV2=IV1+IDV
    ENDIF
    CRZ      IF(MODTRN)THEN
    CRZ          IV1SAV=IV1
    CRZ          IV2SAV=IV2
    CRZ          IDVSAV=IDV
    CRZ      ENDIF
    IF(IV1.NE.0)ALAM1=10000./IV1
    ALAM2=10000./IV2
    IF(IFWHM.LT.1)IFWHM=1
    IF(IFWHM.GT.50)IFWHM=50
    WRITE(IPR,'(17HO FREQUENCY RANGE,/10X,8H   IV1 =,I10,8H CM-1 (,
1     F10.2,13H MICROMETERS),/10X,8H   IV2 =,I10,8H CM-1 (,F10.2,
2     13H MICROMETERS),/10X,8H   IDV =,I10,5H CM-1,/10X,8H IFWHM =,
3     I10,5H CM-1)')IV1,ALAM1,IV2,ALAM2,IDV,IFWHM
    WRITE(IPR,'(15HFREQUENCY RANGE,//10X,9HIV1      =,I11,8H CM-1 (,
1     F7.2,13H MICROMETERS),/10X,9HIV2      =,I11,8H CM-1 (,F7.2,
2     13H MICROMETERS),/10X,9HIDV      =,I11,5H CM-1,/10X,9HIFWHM      =,
3     I11,5H CM-1,/10X,9HIFILTER =,I11)')IV1,ALAM1,IV2,ALAM2,IDV,IFWHM,IFILTER
C
C*****LOAD ATMOSPHERIC PROFILE INTO /MODEL/
C
C      CALL STDMDL
C
C      DEFINE COUNTER ITEST TO PREVENT ZENITH ANGLE QTHETA AND LAYER
C      PATH LENGTH PL FROM BEING CHANGED DURING SOLAR CALCULATIONS
555  DO 15 I=1,102
      DO 15 J=1,KMAX
          WPATH(I,J)=0.0
15  WPATHS(I,J)=0.0
C
C      ITEST=0
C
C      IF (IMULT .EQ. 1) THEN
          H1=ZM(1)
          H2=ZM(ML)
          ITYPE = 2
          ANGLE = 0.
          BETA = 0.
          RANGE =0.
          ISSGS = ISSGEO
          ISSGEO = 0
C
          CALL GEO (IERROR,BENDNG,MAXGEO)
          MSOFF=68
          CALL GEO (IERROR,BENDNG,MAXGEO,MSOFF)
          W15SV = W(15)
C
C      W15SV IS THE REL HUM FROM 0 TO SPACE
C      THIS REL HUM MAY BE DIFFERENT THAN THE PATH REL HUM

```

```

C      WHEN REL HUM ARE DIFFERENT THE ANSWER CAN CHANGE          driv6420
C
C      ISSGEO = ISSGS                                         driv6430
C      IMSMX=IKMAX                                         driv6440
C      DO 35 N=1,IMSMX                                         driv6450
C          PLST(N)=PL(N)                                         driv6460
C          DO 35 K=1,KMAX                                         driv6470
C35      WPMSS(N,K)=WPATH(N,K)                                     driv6480
      35      PLST(N)=PL(N)                                         driv6490
C
C          IF(IEMSCT.EQ.2)  THEN                                     driv6500
C              CALL SSgeo(IERROR,IPH,IPARM,PARM1,PARM2,
C                  PARM3,PARM4,PSIPO,G,MAXGEO)                         driv6510
C                  PARM3,PARM4,PSIPO,G,MAXGEO,MSOFF)                      driv6520
C              DO 30 N=1,IKMAX                                         driv6530
C                  CSENSV(N) = ABS(CSzen(N))                           driv6540
C                  IF(CSENSV(N) .LT. 0.0174) CSENSV(N) = 0.0174           driv6550
      30      CONTINUE                                         driv6560
C              DO 45 N=1,ML                                         driv6570
C              DO 45 K=1,KMAX                                         driv6580
C                  WPMSS(N,K)=WPATHS(N,K)                            driv6590
C 45      CONTINUE                                         driv6600
C          ENDIF                                         driv6610
C
C          ENDIF                                         driv6620
C          H1      = H1S                                         driv6630
C          H2      = H2S                                         driv6640
C          ANGLE   = ANGLES                                       driv6650
C          RANGE   = RANGS                                       driv6660
C          BETA    = BETAS                                       driv6670
C          ITYPE   = ITYPES                                       driv6680
C          LEN     = LENS                                         driv6690
C
C*****TRACE PATH THROUGH THE ATMOSPHERE AND CALCULATE ABSORBER AMOUNTS
C
C          ISSGEO=0                                         driv6700
C          MSOFF=0                                         driv6710
C
C          ***** Save original value of SEA (false if earth not yet hit) *****
C
C          SEAold = SEA                                         driv6720
C          CALL GEO(IERROR,BENDNG,MAXGEO,MSOFF)                   driv6730
C
C          ***** and set HIT true if the earth has been hit within FNDHMN: *****
C          HIT = ((.NOT. SEAold) .AND. SEA)
C          IF (HIT) THEN
C              WRITE (IP6, '(/, 6HSEA AT, F7.2,
C+ 31H K REPLACES BLACK BODY BOUNDARY,/,10X,9HUPWIND =,F11.3,
C+ 26H DEG EAST OF LINE OF SIGHT') TBOUNDold, Psi
C
C          calculate geometry from point of view of the footprint
C          IF (IEMSCTold .EQ. 1) Pr = Psi*d2r + pi
C          IF ((IPARM .EQ. 0) .OR. (IPARM .EQ. 1)) THEN
C              ThetaO = PARM1
C              PhiO   = PARM2
C              ThetaS = PARM3
C              PhiS   = PARM4
C              CALL Foot(ThetaO,PhiO,ThetaS,PhiS,PsiPO,Beta,Psi)
C          ELSE IF (IPARM .EQ. 2) THEN
C              Psi0   = PARM1
C              Del0   = PARM2

```

```

        CALL SunFoot(Psi0,Del0,PsiPO,Beta,Psi)
C      END IF
C      and issue new sky (and sun) cards in file 'TAPE5.SEA'
C      CALL Card
END IF
IF ((SeaSwitch) .AND. (.NOT. Sea)) THEN
    WRITE (IP6, '(/, 13HTBOUND SET TO, F7.2,
+ 17H K FOR MARINE SKY') TBOUND
END IF

C      CALL AERTMP
C      IF(IMULT. NE. 1) W15SV = W(15)                                driv6800
C      SAVE TEMPERATURE AND PATH INFO FOR LATER USE                 driv6810
C
C      IF(IMULT .EQ. 1) THEN                                         driv6820
DO 25 N=1,IKMAX
25   QTHETS(N) = QTHETA(N)                                       driv6830
ENDIF
C
C      IF(IERROR.GT.0) GO TO 630                                     driv6840
IF(IEMSCT.EQ.3 .AND. IERROR.EQ. -5) GO TO 557                  driv6850
GO TO 558
557 CONTINUE
WRITE(IPR,1557)
1557 FORMAT('0 DIRECT PATH TO SUN INTERSECTS THE EARTH: SKIP TO ',
1      'NEXT CASE')
GO TO 630
558 CONTINUE
C
C      IF(IEMSCT.EQ.2)CALL SSGEO(IERROR,IPH,IPARM,PARM1,PARM2,PARM3,
C      1 PARM4,PSIPO,G,MAXGEO)                                      driv7000
C      1 PARM4,PSIPO,G,MAXGEO,MSOFF)                                 driv7010
W(15) = W15SV                                                 driv7020
driv7030
driv7040
driv7050
driv7060
driv7070
driv7080
driv7090
driv7100
driv7110
driv7120
driv7130
driv7140
driv7150
driv7160
driv7180
driv7190
driv7200
driv7170
driv7210
driv7220
driv7230
driv7240
driv7250
C
C      W15SV IS THE REL HUM (FOR MULT SCAT THIS MAY BE DIFFERENT
C      FROM PATH REL HUM)                                         driv7070
C
C      THE SECOND CALL TO SSGEO IS TO GET THE CORRECT ANGLES FOR
C      PHASE FUNCTIONS                                           driv7080
C
C      SAVE SOLAR PATH INFORMATION                               driv7090
C
C      IF(IERROR.GT.0) GO TO 630                                driv7100
C
C      IF(IMULT.EQ.1) THEN                                     driv7110
DO 60 IK = 1,IMSMX
    PL(IK)=PLST(IK)
    IF(IEMSCT.EQ.2) CSZEN(IK)=CSENSV(IK)
60   CONTINUE
    DO 70 IK = 1,IKMAX
70       QTHETA(IK) = QTHETS(IK)
ENDIF
C
C*****LOAD AEROSOL EXTINCTION, ABSORPTION, AND ASYMMETRY COEFFICIENTS
C
CALL EXABIN

```

```

C                                         driv7260
C*****WRITE HEADER DATA TO TAPE 7          driv7270
C                                         driv7280
C560  WRITE(IPU,1110)MODEL,ITYPE,IEMSCT,IMULT,M1,M2,M3,      driv7290
C     1   M4,M5,M6,MDEF,IM,NOPRT,TBOUND,SALB          driv7300
560  WRITE(IPU,'(L1,I4,12I5,F8.3,F7.2)')MODTRN,MODEL      driv7310
     1   ,ITYPE,IEMSCT,IMULT,M1,M2,M3,M4,M5,M6,MDEF,IM,NOPRT,TBOUND,SALB driv7320
C     WRITE(IPR1,1110)MODEL,ITYPE,IEMSCT,IMULT,M1,M2,M3,      driv7330
C     1   M4,M5,M6,MDEF,IM,NOPRT,TBOUND,SALB          driv7340
     WRITE(IPR1,'(L1,I4,12I5,F8.3,F7.2)')MODTRN,MODEL      driv7350
     1   ,ITYPE,IEMSCT,IMULT,M1,M2,M3,M4,M5,M6,MDEF,IM,NOPRT,TBOUND,SALB driv7360
     WRITE(IPU,1200)IHAZE,ISEASN,IVULCN,ICSTL,ICLD,IVSA,VIS,WSS,WHH,      driv7370
     1   RAINRT,GNDALT          driv7380
     WRITE(IPR1,1200)IHAZE,ISEASN,IVULCN,ICSTL,ICLD,IVSA,VIS,WSS,WHH,      driv7390
     1   RAINRT,GNDALT          driv7400
     WRITE(IPU,1210) CTHIK,CALT,CEXT,ISEED          driv7410
     WRITE(IPR1,1210) CTHIK,CALT,CEXT,ISEED          driv7420
     WRITE(IPU,1230)ZCVSA,ZTVSA,ZINVSA          driv7430
     WRITE(IPR1,1230)ZCVSA,ZTVSA,ZINVSA          driv7440
     WRITE(IPU,1255) ML,(HMODEL(I,7),I=1,5)          driv7450
     WRITE(IPR1,1255) ML,(HMODEL(I,7),I=1,5)          driv7460
1255  FORMAT( I5,18A4)          driv7470
     IF(MODEL.NE.0)WRITE (IPU,1312) H1,H2,ANGLE,RANGE,BETA,RO,LEN      driv7480
     IF(MODEL.NE.0)WRITE (IPR1,1312) H1,H2,ANGLE,RANGE,BETA,RO,LEN      driv7490
     HMDLZ(8) = RANGE          driv7500
     IF(MODEL.EQ.0) WRITE(IPU,1560)(HMDLZ(K),K=1,8)          driv7510
     IF(MODEL.EQ.0) WRITE(IPR1,1560)(HMDLZ(K),K=1,8)          driv7520
1560  FORMAT(3F10.3,5E10.3)          driv7530
     WRITE(IPU,1320) IPARM,IPH,IDAY,ISOURC          driv7540
     WRITE(IPR1,1320) IPARM,IPH,IDAY,ISOURC          driv7550
     WRITE(IPU,1322) PARM1,PARM2,PARM3,PARM4,GMT,PSIPO,ANGLEM,G
     WRITE(IPR1,1322) PARM1,PARM2,PARM3,PARM4,GMT,PSIPO,ANGLEM,G
     WRITE(IPU,1400) V1,V2,DV          driv7580
     WRITE(IPR1,1400)V1,V2,DV          driv7590
     WRITE(IPU,'(5I10)')IV1,IV2,IV3,IFWHM,IFILTER
     WRITE(IPR1,'(5I10)')IV1,IV2,IV3,IFWHM,IFILTER
     CRZ  IRAIN=0          driv7620
     CRZ  IF(RAINRT.GT.0) IRAIN=1          driv7630
     CCC  CALCULATE EQUIVALENT LIQUID WATER CONSTANTS          driv7640
     CCC  driv7650
     CALL EQULWC          driv7660
     IF (SEA) THEN          driv7670
        Msea = Msea + 1
        Done = (((IEMSCTold .EQ. 1) .AND. (Msea .EQ. 3))
        +       .OR. ((IEMSCTold .EQ. 2) .AND. (Msea .EQ. 4)))
        IF (Done) THEN
           READ(IRD, 1600) IRPT
        ELSE
           READ(IRDS,1600) IRPT
        END IF
     ELSE
        READ(IRD, 1600) IRPT
     END IF
1600  FORMAT(I5)          driv7720
     WRITE(IPU,1600) IRPT          driv7730

```

```

        WRITE(IPR1,1600) IRPT                         driv7740
C
C     ground=.false.
C     if(h2.le.zm(1))ground=.true.
C     IF (Msea .GT. -1)
+       PRINT '(35H Driver: Calling TRANS for sea card, I2, 1H.)',Msea
        CALL TRANS(IPH,ISOURC,IDAY,ANGLEM,ground)           driv7750
C
C     TRANS RETURNS IRPT = -4 IF THE SPECTRAL RANGE EXTENDS BEYOND THE      driv7760
C     BAND MODEL TAPE. IN THIS CASE, A LOWTRAN 7 CALCULATION IS             driv7770
C     PERFORMED FOR THE SHORT WAVELENGTHS AND THEN THE ORIGINAL INPUT      driv7790
C     IS RESTORED. (NOTE: THIS FEATURE WAS COMMENTED OUT.)                  driv7800
C
C     ***** Reset the parameters to their original values *****
C     ***** from before TAPE5.SEA was introduced, provided *****
C     ***** all cards from TAPE5.SEA have been read. *****
C
C     IF (Done) THEN
C       CLOSE (IRDS, STATUS='KEEP')
C       Sea      = .FALSE.
C       SeaOld   = .FALSE.
C       Hit      = .FALSE.
C       Msea     = -1
C       ITYPE    = ITYPEold
C       IEMSCT   = IEMSCTold
C       IMULT    = IMULTold
C       TBOUND   = TBOUNDold
C       SALB     = SALBold
C
C     END IF
C
C     *****WRITE END OF FILE ON TAPE 7
C
630   IF(IERROR .GT. 0) THEN
C       READ(IRD,1600,END=900) IRPT
C       WRITE(IPU,1600) IRPT
C       WRITE(IPR1,1600) IRPT
C
C     ENDIF
C     WRITE(IPU,1620)
C     WRITE(IPR1,1620)
1620  FORMAT(' -9999.')
C
C     WRITE(IPR,1630) IRPT
1630  FORMAT('0 CARD 5 *****',I5)
C     IF (IRPT.EQ.0) GO TO 900
C     IF (IRPT.EQ.4) GO TO 400
cssi  IF (IRPT.GT.1 .AND. IEMSCT.EQ.3) THEN
cssi  PRINTg1,'/!! ERROR IN INPUT IEMSCT EQ 3 IRPT GT 1!'
cssi  STOP
cssi  ENDIF
C     IF (IRPT.GT.4) GO TO 900
C     GO TO (100,900,300,400), IRPT
900   Call Timer(Iend)
C     to find how long the calculation took:
C     WRITE (ITM, 1880) (FLOAT(Iend)-FLOAT(Istart))/100.
1880  FORMAT ('Elapsed time (sec) for the last run was ', F8.2)
C     STOP
C

```

driv7740
driv7750
driv7760
driv7770
driv7790
driv7800
driv7810
driv7820
driv7840
driv8050
driv8060
driv8070
driv8080
driv8090
driv8100
driv8110
driv8120
driv8130
driv8140
driv8150
driv8160
driv8170
driv8180
driv8190
driv8200
driv8210
driv8220
driv8230
driv8240
driv8250
driv8260

APPENDIX C
MODIFIED SUBROUTINE "TRANS"

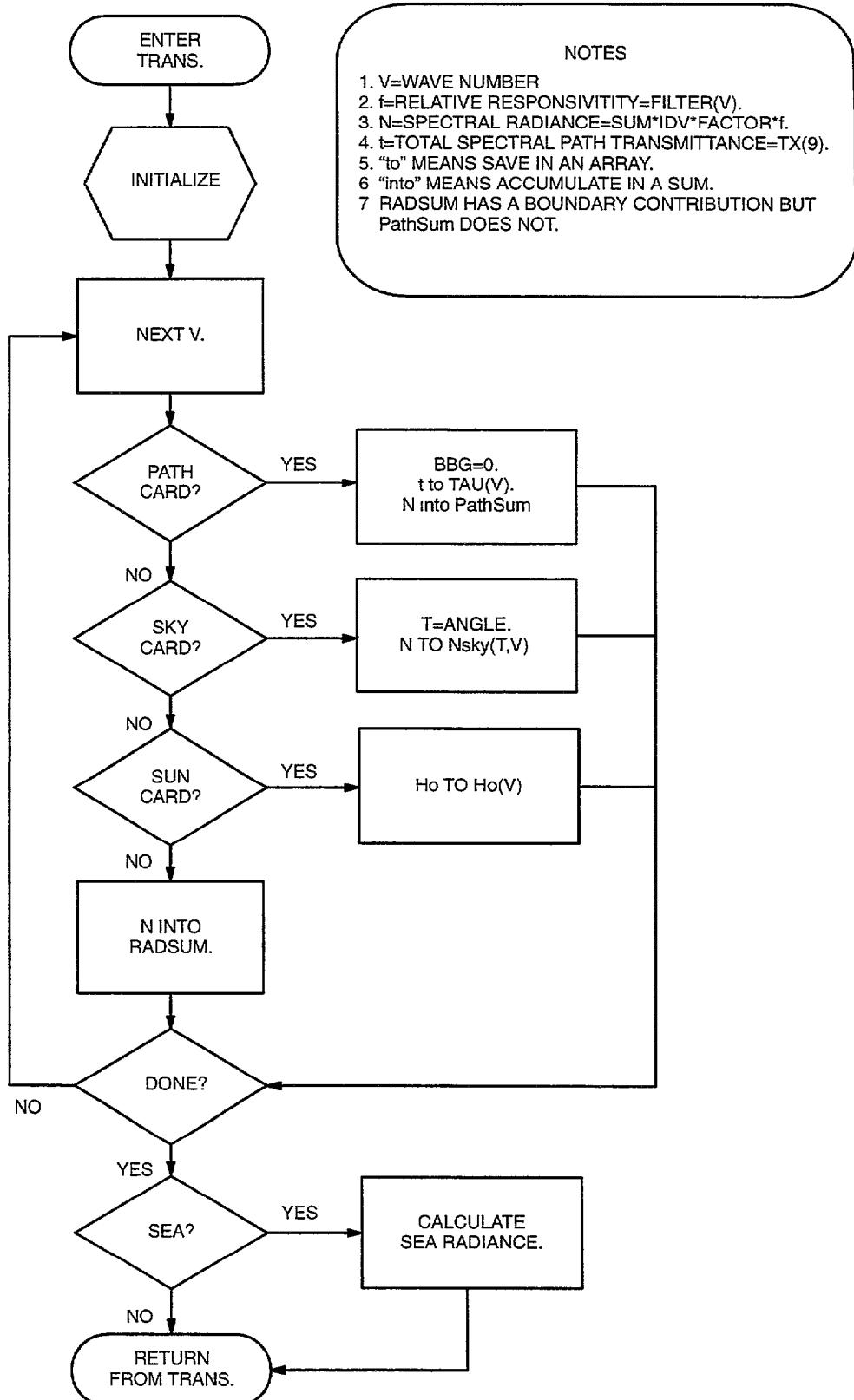


Figure C-1. Flowchart for modified subroutine "TRANS."

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SUBROUTINE TRANS(IPH,ISOURC>IDAY,ANGLEM,ground)
C CALCULATES TRANSMITTANCE AND RADIANCE VALUES BETWEEN IV1 AND IV2
C FOR A GIVEN ATMOSPHERIC SLANT PATH
parameter(nbins=99,iprint=50,maxv=50000)           tras 110
real WGT(nbins),SLIT(56,nbins)                     tras 120
LOGICAL IVTEST,loop0,ground,transm,modtrn          tras 130
COMMON RELHUM(34),WHNO3(34),ICH(4),VH(17),TX(63),W(63),IMSMX,   tras 140
1 WPATH(102,63),TBBY(102),PATM(102),NSPEC,KPOINT(12),           tras 150
2 ABSC(5,47),EXTC(5,47),ASYM(5,47),VX0(47),AWCCON(5)          tras 160
COMMON /IFIL/ IRD,IPR,IPU,NPR,IPR1,IP6,IP7,IP8,IP4,IRDS,IP6S,   tras 170
+ ITR,Isky,Isun,Ipath                                     tras 180
COMMON/CARD1/MODEL,ITYPE,IEMSCT,M1,M2,M3,IM,NOPRNT,TBOUND,SALB,  tras 190
1 MODTRN                                              tras 210
COMMON /CARD2/ IHAZE,ISEASN,IVULCN,ICSTL,ICIR,IVSA,VIS,WSS,WHH,  tras 220
1 RAINRT
COMMON/CARD3/H1,H2,ANGLE,RANGE,BETA,REE,LEN
COMMON/CARD4/IV1,IV2,IDV,IFWHM,IFILTER
COMMON/CNSTNS/PIX,CA,DEG,GCAIR,BIGNUM,BIGEXP
COMMON/CNTRL/KMAX,M,IKMAX,NL,ML,IKLO,ISSGEO,IMULT
COMMON/SOLS/AH1(68),ARH(68),
1 WPATHS(102,63),PA(68),PRX(68),ATHETA(35),ADBETA(35),LJ(69),tras 250
2 JTURB,ANGSUN,CSZEN(68),TBBYS(102,12),PATMS(102,12)           tras 260
COMMON/SRAD/TEB1,TEB2SV
COMMON/MSRD/TLE(34),COSBAR(34),OMEGA0(68),UPF(10,34),DNF(10,34),
1 TAER(34),ASYIK(68),ASYDM(68),STRN(0:34),DMOLS(68),DSTRN(0:68),tras 280
2 FDNSRT,FDNTRT,TAUT(34),UMF(34),DMF(34),UMFS(34),DMFS(34)      tras 290
COMMON/ICLL/ICALL,FPHS,FALB,FORBIT
PARAMETER (Kr = 216, Kv = 400)
COMMON /Filters/ FLIST(5,6),
+ FILTER1(45), BB1(Kr), FILTER2(54), BB2(Kr),
+ FILTER3(39), BB3(Kr), FILTER4(47), BB4(Kr),
+ FILTER5(101),BB5(Kr), FILTER6(75), BB6(Kr)
COMMON/Sea/ Sea,Hit,Msea,TBOUNDold,IEMSCTold
COMMON/Geometry/ To,Po,Tr,Pr
COMMON/Constants/pi,r2d,d2r,epsilon,delta,one,m,onep,infinity
DIMENSION Tau(Kv), SkyN(3,Kv), Ho(Kv), Tsky(3), Rsky(3)
LOGICAL Sea, PathCard, SkyCard, LastSky, SunCard, Hit
REAL Npath, Nsky, Nvsky, Nsea, Nsun, Ntotal, Nbb, infinity, No
TO = 273.15
common /solar/lsame                                         tras 340
logical lsame                                              tras 350
c Initialize slit function array                           tras 360
DO 10 I = 1,56                                         tras 370
    DO 10 J = 1,nbins                                    tras 380
10 SLIT(I,J) =0.                                         tras 390
c Initialize radiance minimum and maximum parameters   tras 400
RADMIN=bignum                                           tras 410
RADMAX=0.                                                 tras 420
c Initialize ground emissivity (one minus ground albedo) tras 430
EMISS=1.-SALB                                           tras 440
c Store the number of path layers in ikmx               tras 450
IKMX=IKMAX                                              tras 460
trias 470
tras 480
tras 490
tras 500

```

```

c          tras 510
c Initialize integrated absorption, radiance, solar irradiance and tras 520
c transmitted solar irradiance sums tras 530
c SUMA=0. tras 540
c RADSUM=0. tras 550
c SSOL=0. tras 560
c STSOL=0. tras 570
c PathSum = 0.
c PathCard = .FALSE.
c SkyCard = .FALSE.
c LastSky = .FALSE.
c SunCard = .FALSE.
c IF (Sea) THEN
c   IF (Msea .EQ. 0) THEN
c     PathCard = .TRUE.
c   ELSE IF ((Msea .GE. 1) .AND. (Msea .LE. 3)) THEN
c     SkyCard = .TRUE.
c   ELSE IF (Msea .EQ. 4) THEN
c     SunCard = .TRUE.
c   END IF
c   IF (Msea .EQ. 3) THEN
c     LastSky = .TRUE.
c   END IF
c END IF
c IF (SkyCard) Tsky(Msea) = ANGLE*d2r
c Istore = 0
c          tras 580
c Initialize integration weighting factor tras 590
c FACTOR=.5 tras 600
c          tras 610
c Initialize icount, used to determine when header must be printed tras 620
c ICOUNT=iprint tras 630
c          tras 640
c Do not perform a MODTRAN calculation if all sources are continuum tras 650
cssi  IF(IV1.GE.22655)modtrn=.false.
      IF(IV1.GE.22681)modtrn=.false.
      IF(modtrn)THEN
c          tras 660
c          tras 670
c          tras 680
c          tras 690
c WHEN THE band model or line-by-line option is used, call tras 700
c routine "bmdata" to INITIALIZE PARAMETERS AND TO SET THE tras 710
c FREQUENCY STEP SIZE "IDVX" TO THE BAND WIDTH (1 CM-1). tras 720
c IDV5=5 tras 730
c CALL bmdata(IV1,IFWHM,IDVX,IKMX,MXFREQ)
c IWIDM1=IFWHM/IDVX-1 tras 740
c IV=5*((IV1-IWIDM1)/5) tras 750
c IF(IV.LT.0)IV=0 tras 760
c IVX=IV-IDVX tras 770
c IV=IV-5 tras 780
c IVXMAX=IV2+IWIDM1 tras 790
c          tras 800
c ELSE
c   IDV5=IDV tras 810
c   IDVX=IDV5 tras 820
c   IWIDM1=0 tras 830
c   IV=IV1-IDV5 tras 840
c   IVX=IV tras 850
c   IVXMAX=IV2+IWIDM1 tras 860
c   IF(IVXMAX.GT.maxv) IVXMAX=maxv
c          tras 870
c          tras 880

```

```

      IF(IDV.LT.5) IDV=5                               tras 890
      ENDIF                                              tras 900
      IWRITE=IV1+IWIDM1                                tras 910
      IWIDTH=IWIDM1+1                                  tras 920
C
C      PERFORM TRIANGULAR SLIT INITIALIZATION. TRANSMITTANCES AT A   tras 930
C      GIVEN FREQUENCY CONTRIBUTE TO 2*IWIDTH-1 TRIANGULAR SLITS.   tras 940
C      THESE CONTRIBUTIONS ARE STORED IN ARRAY SLIT. WGT IS THE   tras 950
C      NORMALIZED WEIGHT USED TO DEFINE THE TRIANGLE.               tras 960
      NWGT=2*IWIDTH                                     tras 970
      WNORM=1./(IWIDM1*IWIDTH)                           tras 980
      DO 20 I=1,IWIDTH                                 tras 990
         WGT(I)=I*WNORM                               tras1000
20     WGT(NWGT-I)=wgt(i)                            tras1010
      NWGT=NWGT-1                                    tras1020
      NWGTM1=NWGT-1                                  tras1030
C
C      Initialize ICALL (= 0 for initial call to subroutine source)   tras1040
      ICALL=0                                         tras1050
C
C      Initialize transm (.true. for transmittance only calculations)   tras1060
      transm=.true.                                    tras1070
      IF(IEMSCT.EQ.1 .OR. IEMSCT.EQ.2)transm=.false.   tras1080
C
C      Print headers                                     tras1090
      IF(IEMSCT.EQ.0)THEN
        WRITE(IPU,'(46H \FREQ TOTAL H2O CO2+ OZONE TRACE,tras1150
1       49H N2 CON H2O CON MOL SCAT AER-HYD HNO3 AER-HYD')')    tras1160
        WRITE(IP7,'(46H \FREQ TOTAL H2O CO2+ OZONE TRACE,
1       49H N2 CON H2O CON MOL SCAT AER-HYD HNO3 AER-HYD')')
        WRITE(IPR1,'(45H \FREQ H2O O3 CO2 CO CH4,tras1170
1       47H N2O O2 NH3 NO NO2 SO2,/ tras1180
2       55H \1/CM TRANS TRANS TRANS TRANS TRANS, tras1190
3       39H TRANS TRANS TRANS TRANS TRANS )')
        WRITE(IP8, '(45H \FREQ H2O O3 CO2 CO CH4,
1       47H N2O O2 NH3 NO NO2 SO2,/ 
2       55H \1/CM TRANS TRANS TRANS TRANS TRANS, 
3       39H TRANS TRANS TRANS TRANS TRANS )')
      ELSE IF(IEMSCT .EQ. 3) THEN                      tras1210
        WRITE (IPU,'(32H \FREQ TRANS SOL TR SOLAR)')      tras1220
        WRITE (IP7,'(2H \, T25,
+          40HIRRADIANCE (W M-2) PASSED THROUGH FILTER,
+          I2)') IFILTER
        WRITE (IP7,'(32H \FREQ TRANS SOL TR SOLAR)')
      ELSE IF (IEMSCT .EQ. 1) THEN                     tras1230
        WRITE(IPU,'(45H \FREQ TRANS ATMOS. RAD., T88,
+          18H- LOG TOTAL TRANS.)')
        WRITE(IP7,'(2H \, T25,
+          43HRADIANCE (W M-2 SR-1) PASSED THROUGH FILTER,
+          I2)') IFILTER
        WRITE(IP7,'(30H \FREQ TRANS ATMOS. RAD., T88,
+          18H- LOG TOTAL TRANS.)')
      ELSE IF (IEMSCT .EQ. 2) THEN                     tras1240
        WRITE(IPU,'(42H \FREQ TRANS ATMOS PATH SINGLE,
1       28H GROUND DIRECT TOTAL RAD)')                tras1250
        WRITE(IP7,'(2H \, T25,
+          43HRADIANCE (W M-2 SR-1) PASSED THROUGH FILTER,

```

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+
+           I2')') IFILTER
+      WRITE(IP7,'(42H \FREQ   TRANS     ATMOS    PATH      SINGLE,
1      28H   GROUND DIRECT   TOTAL RAD, T88,
+      18H- LOG TOTAL TRANS.')')
END IF
If (PathCard) then
      WRITE(IPPath,'(1H\, T25,
+      52HRADIANCE (W M-2 SR-1 (CM-1)-1) PASSED THROUGH FILTER,
+      I2,/,1H\,/,40H\ V   T   f   Npath*f   INTEGRAL,
+      /,1H\')') Ifilter
Else if (LastSky) then
      WRITE(Isky,'(1H\, T25,
+      52HRADIANCE (W M-2 SR-1 (CM-1)-1) PASSED THROUGH FILTER,
+      I2,/,1H\,/,40H\ V   T   f   Nsky*T*f   INTEGRAL,
+      22H  Nsea*T*f   INTEGRAL,/,1H\')') Ifilter
Else if (SunCard) then
      WRITE(Isun,'(1H\, T25,
+      52HRADIANCE (W M-2 SR-1 (CM-1)-1) PASSED THROUGH FILTER,
+      I2,/,1H\,/,40H\ V   T   f   Nsun*T*f   INTEGRAL,
+      /,1H\')') Ifilter
End If
IF(NOPRNT.EQ.-1)THEN
  IF(IMULT.EQ.1)THEN
    WRITE(IPR1,'(37H      \V   ALT1      UFLX      UFLXS,      tras1270
1      50H       DFLX      DFLXS      DIRS      TRANS')tras1280
    WRITE(IP8, '(37H      \V   ALT1      UFLX      UFLXS,      tras1290
1      50H       DFLX      DFLXS      DIRS      TRANS')tras1300
  ELSE
    IF(IEMSCT.GT.0)WRITE(IPR1,'(23H      \V   ALT1      ALT2,      tras1310
1      30H       B(V,T)    DTAU      TAU')tras1320
    WRITE(IP8, '(23H      \V   ALT1      ALT2,      tras1330
1      30H       B(V,T)    DTAU      TAU')tras1340
  ENDIF
ENDIF
C
C Initialize layer loop variables
loop0=.true.
call loop(loop0,iv,ivx,ikmx,mxfreq,summs,transm,iph,
1 sumssr,ivtest,unif,trace,sumv,isourc,iday,anglem,frac)
loop0=.false.
C
C END INITIALIZATION, BEGIN OF FREQUENCY LOOP
C
C "IVX" IS THE FREQUENCY AT WHICH TRANSMITTANCE WILL BE CALCULATED. tras1450
C DURING THE FIRST PASS, "IVX" AND "IV" MUST BE EQUAL. tras1460
30 IVX=IVX+IDVX
  IF(IV.LT.IVX)THEN
    IV=IV+IDV5
    IVTEST=.TRUE.
  ELSE
    IVTEST=.FALSE.
  ENDIF
C
C SET INTERPOLATION FRACTION.
FRAC=FLOAT(IV-IVX)/IDV5
IF(ICOUNT.EQ.iprint)THEN
C

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c      Reinitialize counter and print header           tras1590
1      ICOUNT=0                                     tras1600
2      IF(IEMSCT.EQ.0)THEN                         tras1610
3          WRITE(IPR,'(1H1,/33H FREQ WAVELENGTH TOTAL H2O,tras1620
4              47H CO2+ OZONE TRACE N2 CONT H2O CONT, tras1630
5              47H MOL SCAT AER-HYD HNO3 AER-HYD INTEGRATED, tras1640
6              //43H 1/CM MICRONS TRANS TRANS TRANS,   tras1650
7              44H TRANS TRANS TRANS TRANS,           tras1660
8              40H TRANS TRANS ABS ABSORPTION,/)')  tras1670
9      ELSEIF(IEMSCT.EQ.1)THEN                      tras1680
1          WRITE(IPR,'(1H1,20X,28HRADIANCE(WATTS/CM2-STER-XXX),tras1690
2              /8H0 FREQ,T10,6HWAVLEN,T19,14HATMOS RADIANCE,tras1700
3              T39,9H INTEGRAL,T49,5HTOTAL,/2X,6H(CM-1),tras1710
4              T10,7H(MICRN),T19,6H(CM-1),T29,7H(MICRN),tras1720
5              T39,6H(CM-1),T49,5HTRANS,/)')  tras1730
6      ELSEIF(IEMSCT.EQ.3)THEN                      tras1740
7          WRITE(IPR,'(1H1,22X,27HIRRADIANC (WATTS/CM2-XXXX),tras1750
8              /7H0 FREQ,T11,6HWAVLEN,T23,11HTRANSMITTED,tras1760
9              T45,5HSOLAR,T61,10HINTEGRATED,T80,5HTOTAL,tras1770
10             /2X,6H(CM-1),T10,7H(MICRN),T20,6H(CM-1),tras1780
11             T30,7H(MICRN),T40,6H(CM-1),T50,7H(MICRN),tras1790
12             T60,6HTRANS.,T70,5HSOLAR,T80,5HTRANS)')  tras1800
13      ELSEIF(IMULT.EQ.0)THEN                      tras1810
14          WRITE(IPR,'(1H1,45X,28HRADIANCE(WATTS/CM2-STER-XXX),tras1820
15              /7H0 FREQ,T11,6HWAVLEN,T21,14HATMOS RADIANCE,tras1830
16              T41,14HPATH SCATTERED,T61,16HGROUND REFLECTED,tras1840
17              T85,5HTOTAL,T99,8HINTEGRAL,T110,5HTOTAL,tras1850
18              /2X,6H(CM-1),T10,7H(MICRN),T20,6H(CM-1),tras1860
19              T30,7H(MICRN),T40,6H(CM-1),T50,7H(MICRN),tras1870
20              T60,6H(CM-1),T70,7H(MICRN),T80,6H(CM-1),tras1880
21              T90,7H(MICRN),T100,6H(CM-1),T110,5HTRANS,/)')  tras1890
22      ELSE                                         tras1900
23          WRITE(IPR,'(1H1,45X,28HRADIANCE(WATTS/CM2-STER-XXX),tras1910
24              //6H0 FREQ,T10,6HWAVLEN,T20,14HATMOS RADIANCE,T40,tras1920
25              4HPATH,19H SCATTERED RADIANCE,T69,tras1930
26              25HGROUND REFLECTED RADIANCE,T100,14HTOTAL RADIANCE,tras1940
27              T118,8HINTEGRAL,T127,5HTOTAL,/T45,5HTOFFL,T59,tras1950
28              6HS SCAT,T75,5HTOTAL,T89,6HDIRECT,/1X,6H(CM-1),T9,tras1960
29              7H(MICRN),T19,6H(CM-1),T29,7H(MICRN),T39,6H(CM-1),tras1970
30              T49,7H(MICRN),T59,6H(CM-1),T69,6H(CM-1),T79,tras1980
31              7H(MICRN),T89,6H(CM-1),T99,6H(CM-1),T109,7H(MICRN),tras1990
32              T119,6H(CM-1),T127,5HTRANS,/)')  tras2000
33      ENDIF                                         tras2010
34  ENDIF                                         tras2020
c      Determine layer loop maximum               tras2030
c      IF(transm)THEN                           tras2040
c          FOR transmission calculations, skip over layer loop in tratas2070
c              IKMAX=1                           tras2080
c      ELSEIF(IMULT.EQ.1 .and. .not. lsame)THEN  tras2090
c          FOR MULTIPLE SCATTERING SET IKMAX TO IMSMX  tras2100
c              IKMAX=IMSMX                     tras2110
c      ELSE                                         tras2120
c          IF NOT MULTIPLE SCATTERING, RESET IKMAX TO ORIGINAL VALUE  tras2130
c                                         tras2140
c                                         tras2150

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      IKMAX=IKMX
      ENDIF
      SUMV=0.

C
C      Initialize transmission array
      TX(1)=1.
      TX(2)=1.
      TX(3)=1.
      DO 40 K=4,KMAX
40    TX(K)=0.
      call loop(loop0,iv,ivx,ikmx,mxfreq,summs,transm,
      1      iph,sumssr,ivtest,unif,trace,sumv,isourc,iday,anglem,frac)
C
C      THE PARAMETERS "UNIF", "TRACE", "SUMV", "SUMSSR", "SUMMS"
C      AND "TEB1" ARE TEMPORARILY STORED IN "TX" SO THAT THEIR
C      CONVOLUTION OVER THE TRIANGULAR SLIT CAN BE CALCULATED.
      TX(2)=UNIF
      TX(3)=TRACE
      TX(8)=SUMV
      TX(12)=SUMSSR
      TX(13)=SUMMS
      TX(14)=TEB1
      DO 60 K=2,56
      IP1=NWGT
      DO 50 I=NWGTM1,1,-1
      SLIT(K,IP1)=SLIT(K,I)+WGT(IP1)*tx(k)
50    IP1=I
      SLIT(K,1)=WGT(1)*tx(k)
60    TX(K)=SLIT(K,NWGT)

C      CHECK IF VALUES ARE TO BE PRINTED
      IF(IVX.LT.IWRITE)GOTO30
      IWRITE=IWRITE+IDV
      IF(IWRITE.GT.IVXMAX)FACTOR=.5
      ICOUNT=ICOUNT+1

C      RENORMALIZE IF TRIANGULAR SLIT EXTENDS TO NEGATIVE FREQUENCIES
      IF(IVX.LT.NWGTM1)THEN
      store=1.-.5*(NWGTM1-IVX)*(NWGTM1-IVX+1)*WNORM
      DO 70 K=2,56
70    TX(K)=TX(K)/store
      ENDIF
      UNIF=TX(2)
      TRACE=TX(3)
      SUMV=TX(8)
      SUMSSR=TX(12)
      SUMMS=TX(13)
      TEB1=TX(14)
      V=FLOAT(IVX-IWIDM1)
      ALAM=1.0E+04/(V+.000001)
      Istore = Istore + 1
      Width = IDV*FACTOR
      f = Filter(V,Ifilter)
      SUMA=SUMA+(1.0-TX(9))*f*Width
      ALTX9=BIGNUM
      IF(TX(9).GT.0.)ALTX9=-LOG(TX(9))
      GOTO(80,90,90,100),IEMSCT+1

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C          TRANSMITTANCE ONLY                               tras2700
C          TX(10)=1.-TX(10)                                tras2710
C          TX(7)=TX(7)*TX(16)                              tras2720
C          WRITE(IPR,'(F8.0,F8.3,11F9.4,F12.3)')V,ALAM,TX(9),TX(17),tras2730
C          UNIF,TX(31),TRACE,TX(4),TX(5),TX(6),TX(7),TX(11),TX(10),SUMATras2750
C          WRITE(IPR1,'(F7.0,11F8.4,1PE10.3)')V,TX(17),TX(31),TX(36),tras2760
C          TX(44),TX(46),TX(47),TX(50),TX(52),TX(54),TX(55),TX(56)tras2770
C          WRITE(IP8,'(F7.0,11F8.4,1PE10.3)')V,TX(17),TX(31),TX(36),
C          TX(44),TX(46),TX(47),TX(50),TX(52),TX(54),TX(55),TX(56)
C          WRITE(IPU,'(F7.0,11F8.4,1PE10.3)')V,TX(9),TX(17),UNIF,
C          TX(31),TRACE,TX(4),TX(5),TX(6),TX(7),TX(11),TX(10),ALTX9tras2780
C          WRITE(IP7,'(F7.0,11F8.4,1PE10.3)')V,TX(9),TX(17),UNIF,
C          TX(31),TRACE,TX(4),TX(5),TX(6),TX(7),TX(11),TX(10),ALTX9tras2790
C          GOTO110                                         tras2800
C
C          ATMOSPHERIC RADIANCE INCLUDING EMISSION OF BOUNDARY      tras2810
C          ATTENUATED BY TOTAL TRANSMISSION                         tras2820
C
C          CALCULATE THERMAL RADIANCE CONTRIBUTION OF BOUNDARY AND      tras2840
C          ADD THE SCATTERED CONTRIBUTION TO THE THERMAL RADIANCE      tras2850
C          IF THE PATH INTERSECTS THE SURFACE                         tras2860
C
C          90 IF ((TBOUND.LE.0.) .OR. (PathCard)) THEN           tras2870
C                  BBG = 0.                                         tras2890
C          ELSE                                                 tras2900
C                  BBG=BBFN(TBOUND,V)*TX(9)*EMISS                 tras2910
C                  IF (IMULT.EQ.1 .AND. ground) THEN               tras2920
C                      BBG=BBG+SALB*FDNTRT*TX(9)/PI
C                  END IF                                         tras2930
C          ENDIF                                              tras2940
C
C          ADD THERMAL BOUNDARY AND MULTIPLE SCATTERED RADIANCE      tras2950
C          SUMV=(SUMV+BBG)*f                                     tras2970
C          SUMVV=SUMV
C          IF (V.GT.0.) THEN
C              SUMV=(1.0E+08/V**2)*SUMV                         ! W m-2 sr-1 (cm-1)-1
C          END IF
C          IF (IEMSCT.EQ.1)THEN
C              RADSUM=RADSUM + SUMV*Width                     tras2990
C              WRITE(IPR,'(F8.0,F8.3,1P3E10.2,0PF9.4)')
C              V,ALAM,SUMV,SUMVV,RADSUM,TX(9)                tras3010
C              WRITE(IPU,'(F7.0,F8.4,1PE15.8,T96,E10.3)')
C              V,TX(9),SUMV,ALTX9                            tras3030
C              WRITE(IP7,'(F7.0,F8.4,1PE15.8,T96,E10.3)')
C              V,TX(9),SUMV,ALTX9                            tras3040
C              WRITE(IPR1,'(F7.0,11F8.4,1PE10.3)')V,TX(9),TX(17),UNIF,tras3050
C              TX(31),TRACE,TX(4),TX(5),TX(6),TX(7),TX(11),TX(10),ALTX9tras3060
C              WRITE(IP8,'(F7.0,11F8.4,1PE10.3)')V,TX(9),TX(17),UNIF,
C              TX(31),TRACE,TX(4),TX(5),TX(6),TX(7),TX(11),TX(10),ALTX9
C              SUMTT=SUMV
C              SUMTT=SUMVV                                         tras3070
C          ELSE
C              SOLAR SCATTERED RADIANCE                         tras3080
C              CALL SOURCE(V,ISOURC,IDAY,ANGLEM,SS)            tras3090
C
C              MULTIPLY SUMSSR BY THE EXTRATERRESTRIAL SOURCE STRENGTH SStras3140

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C          SUMSSS=SUMSSR*SS                               tras3150
C          CALCULATE TOTAL SINGLE SCATTERED + MULTIPLE SCATTERED tras3160
C          SOLAR RADIANCE FOR EACH FREQUENCY [W/CM2-STER-MICROMETER] tras3170
C          SUMSSR=SUMSSS+SUMMS                                tras3180
C          store=0.                                         tras3190
C          if(v.gt.0.)store=1.e8/v**2           ! [W m-2 sr-1 (cm-1)-1] tras3200
C          SUMS=store*SUMSSR                         tras3220
C          SUMSSS=store*SUMSSS                         tras3230
C          RFLSOL IS GROUND-REFLECTED DIRECT SOURCE RADIANCE AND tras3240
C          RFLSOL=0.                                     tras3250
C          RFLS=0.                                       tras3260
C          RFLSS=0.                                     tras3270
C          RFLSSS=0.                                    tras3280
C          IF(ground .AND. TEB1.GT.0)THEN               tras3290
C              IF(ANGSUN.GE.0.)RFLSSS=SS*TEB1*SALB*COS(ANGSUN*CA)/PI tras3310
C              RFLSOL=RFLSSS                         tras3320
C              IF(IMULT.EQ.1)RFLSOL=RFLSOL+SALB*FDNSRT*TX(9)/PI tras3330
C              RFLS=STORE*RFLSOL                         tras3340
C              RFLSS=STORE*RFLSSS                         tras3350
C          ENDIF                                         tras3360
C          SUMT=SUMV+(SUMS+RFLS)*f
C          SUMTT=SUMVV+(SUMSSR+RFLSOL)*f
C          RADSUM=RADSUM + SUMT*Width
C          IF (IMULT.NE.1) THEN                           tras3400
C              WRITE(IPR,'(F8.0,F8.3,1P9E10.2,0PF9.4)')
C              V,ALAM,SUMV,SUMVV,SUMS,SUMSSR,RFLS,RFLSOL,      tras3410
C              SUMT,SUMTT,RADSUM,TX(9)                      tras3420
C          ELSE                                           tras3430
C              WRITE(IPR,'(F7.0,F8.3,1P11E10.2,0PF7.4)')
C              V,ALAM,SUMV,SUMVV,SUMS,SUMSSR,SUMSSS,RFLS,      tras3440
C              RFLSOL,RFLSS,SUMT,SUMTT,RADSUM,TX(9)          tras3450
C          END IF                                         tras3460
C          WRITE(IPU,'(F7.0,F8.4,1P6E9.2,0P2F8.4,T96,1PE10.3)')V,      tras3470
C          TX(9),SUMV,SUMS,SUMSSS,RFLS,RFLSS,SUMT,TEB1,TEB2SV,ALTX9tras3500
C          WRITE(IP7,'(F7.0,F8.4,1P6E9.2,0P2F8.4,T96,1PE10.3)')V,
C          TX(9),SUMV,SUMS,SUMSSS,RFLS,RFLSS,SUMT,TEB1,TEB2SV,ALTX9
C          WRITE(IPr1,'(F7.0,11F8.4,1PE10.3)')V,TX(9),TX(17),UNIF,      tras3510
C          TX(31),TRACE,TX(4),TX(5),TX(6),TX(7),TX(11),TX(10),ALTX9   tras3520
C          WRITE(IP8,'(F7.0,11F8.4,1PE10.3)')V,TX(9),TX(17),UNIF,
C          TX(31),TRACE,TX(4),TX(5),TX(6),TX(7),TX(11),TX(10),ALTX9
C      END IF                                         tras3530
C      IF (PathCard) THEN
C          Tau(Istore) = TX(9)
C          PathSum = PathSum + SUMT*Width
C          Write(Ipath, '(I5,2F7.3,2(1PE11.3))')
C          + V, TX(9), f, SUMT, PathSum
C      END IF
C      IF (SkyCard) SkyN(Msea,Istore) = SUMT
C
C          GO TO 110                                     tras3540
C
C          DIRECTLY TRANSMITTED SOLAR IRRADIANCE [WATTS/(CM2 MICROMETER)]tras3550
C          CALL SOURCE(V,ISOURC,IDAY,ANGLEM,SOLIL)        tras3560
C          SOLIV=0.                                       tras3570
C          IF(V.GT.0.)SOLIV=SOLIL*1.E+8/V**2           ! [W m-2 sr-1 (cm-1)-1] tras3580

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TSOLIV=SOLIV*TX(9)*f
IF (SunCard) then
  Ho(Istore) = TSOLIV
END IF
TSOLIL=SOIL*L*TX(9)*f
STSOL=STSOL+TSOLIV*Width
SSOL=SSOL+SOLIV*Width
WRITE(IPR,'(F8.0,F8.3,1P6E10.2,0PF9.4)')
1   V,ALAM,TSOLIV,TSOLIL,SOLIV,SOLIL,STSOL,SSOL,TX(9)           tras3640
1   WRITE(IPU,'(F7.0,F8.4,1P2E9.2,T96,E10.3)')
1     V, TX(9), TSOLIV, SOLIV, ALTX9                               tras3650
1   WRITE(IP7,'(F7.0,F8.4,1P2E9.2,T96,E10.3)')
1     V, TX(9), TSOLIV, SOLIV, ALTX9                               tras3660
1   WRITE(IPR1,'(F7.0,11F8.4,1PE10.3)')V,TX(9),TX(17),UNIF,
1     TX(31),TRACE,TX(4),TX(5),TX(6),TX(7),TX(11),TX(10),ALTX9    tras3670
1   WRITE(IP8,'(F7.0,11F8.4,1PE10.3)')V,TX(9),TX(17),UNIF,
1     TX(31),TRACE,TX(4),TX(5),TX(6),TX(7),TX(11),TX(10),ALTX9    tras3680
SUMT=TSOLIV
RADSUM=STSOL
110  IF(IEMSCT.NE.0)THEN
      IF(SUMT.GE.RADMAX)THEN
        VRMAX=V
        RADMAX=SUMT
      ENDIF
      IF(SUMT.LE.RADMIN)THEN
        VMIN=V
        RADMIN=SUMT
      ENDIF
      FACTOR=1.
      IF(IWRITE.LE.IVXMAX)GOTO30
C
C  END OF FREQUENCY LOOP
C
IVX=INT(V+.5)
C
IF (IFILTER .EQ. 0) THEN
  Sumf = IVX - IV1
ELSE IF ((1 .LE. IFILTER) .AND. (IFILTER .LE. 6)) THEN
  Sumf = FLIST(5, IFILTER)
END IF

IF ((.NOT. Sea) .AND. ((IEMSCT .EQ. 1) .OR. (IEMSCT .EQ. 2))) THEN
  IF (IFILTER .EQ. 0) THEN
    V1 = FLOAT (IV1)
    V2 = FLOAT (IVX)
    DV = FLOAT (IDVX)
    CALL RtoT (V1, V2, DV, RADSUM/1.E4, BBTEMP)
  ELSE IF ((IFILTER .GE. 1) .AND. (IFILTER .LE. 6)) THEN
    CALL Planck (RADSUM/1.E4, IFILTER, BBTEMP)
  END IF
END IF

IF (Sea) THEN
  IF (PathCard) THEN
    Npath      = PathSum
    PathTrans = 1.-SUMA/Sumf

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PathRange = RANGE
PathAngle = ANGLE
ELSE IF (LastSky) THEN
  DO I = 1, Istore
    DO K = 1, 3
      Rsky(K) = SkyN(K,I)
    END DO
    CALL Fit(Tsky,Rsky,3,a,b)
    V = IV1 + (I - 1.)*IDV
    f = FILTER(V,Ifilter)
    IF ((I .EQ. 1) .OR. (I .EQ. Istore)) THEN
      Width = IDV/2.
    ELSE
      Width = IDV
    END IF
    Nbb = BBFN(TBOUNDold,V)*f*1E8/V**2
    CALL Sky(Tr,Pr,WSS,a,b,V,BoverA,ev,Nsky)
    Nsky = Nsky + Nvsky*Width*Tau(I)
    Nsea = Nsea + ev*Nbb*Width*Tau(I)
    Write(Isky, '(I5, 2F7.3, 4(1PE11.3))')
+      V, Tau(I), f, Nvsky*Tau(I), Nsky,
+      ev*Nbb*Tau(I), Nsea
    END DO
  ELSE IF (SunCard) THEN
    DO I = 1, Istore
      V = IV1 + (I - 1.)*IDV
      f = FILTER(V, Ifilter)
      IF ((I .EQ. 1) .OR. (I .EQ. Istore)) THEN
        Width = IDV/2.
      ELSE
        Width = IDV
      END IF
      CALL Sun(Tr,Pr,WSS,To,Po,V,sum4)
      No = Ho(I)*sum4/(4.*pi*epsilon**2*BoverA)
      Nsun = Nsun + No*Width*Tau(I)
      Write(Isun, '(I5,2F7.3,2(1PE11.3))')
+        V, Tau(I), f, No*Tau(I), Nsun
    END DO
  END IF
  Ntotal = Npath + Nsea + Nsky + Nsun
  IF (IFILTER .EQ. 0) THEN
    V1 = FLOAT (IV1)
    V2 = FLOAT (IVX)
    dV = FLOAT (IDVX)
    CALL RtoT (V1, V2, dV, Ntotal/1.E4, TotalT)
  ELSE IF ((IFILTER .GE. 1) .AND. (IFILTER .LE. 6)) THEN
    CALL Planck (Ntotal/1.E4, IFILTER, TotalT)
  END IF
END IF
C
IF (.NOT. Sea) THEN
  WRITE(IPR,'(26HINTEGRATED ABSORPTION FROM,I5,3H TO,I5,
+    7H CM-1 =,F10.2,5H CM-1,/23HAVERAGE TRANSMITTANCE =,
+    F6.4,/)') IV1,IVX,SUMA,1.-SUMA/Sumf
  WRITE(IP6,'(
+    /24HINTEGRATED ABSORPTION =, F10.2,
+    10H CM-1 FROM, I5, 3H TO, I5, 5H CM-1,

```

tras3880
tras3890

```

+
+      /24HAVERAGE TRANSMITTANCE   =, F12.4)')
+      SUMA,IV1,IVX,1.-SUMA/Sumf
+ IF (IEMSCT .EQ. 0) THEN
+         WRITE(IP4, '(T13,F7.2,F8.3,F10.3,F8.3)')
+             (90.-ANGLE)*pi/180.*1.E3,
+             ANGLE, RANGE, 1.-SUMA/Sumf
+ ELSE IF ((IEMSCT .EQ. 1) .OR. (IEMSCT .EQ. 2)) THEN
+         WRITE(IPR,'(22 HINTEGRATED RADIANCE =,1PE11.3,
+             10H WATTS M-2,7H STER-1,
+             /22H MINIMUM RADIANCE   =,E11.3,10H WATTS M-2,
+             19H STER-1 (CM-1)-1 AT,OPF11.1,5H CM-1,
+             /8H MAXIMUM,14H RADIANCE   =,1PE11.3,
+             29H WATTS M-2 STER-1 (CM-1)-1 AT,OPF11.1,5H CM-1,
+             23H BOUNDARY TEMPERATURE   =, F11.2,2H K,
+             /22H BOUNDARY EMISSIVITY =,F12.3)')
+             RADSUM,RADMIN,VRMIN,RADMAX,VRMAX,TBOUND,EMISS      tras4020
+         WRITE(IP6,'(
+             /24HMAXIMUM RADIANCE   =, 1PE11.3,
+             23H W M-2 SR-1 (CM-1)-1 AT, OPF8.1, 5H CM-1,
+             /24HMINIMUM RADIANCE   =, 1PE11.3,
+             23H W M-2 SR-1 (CM-1)-1 AT, OPF8.1, 5H CM-1,
+             /24HBOUNDARY TEMPERATURE   =, F11.2, 2H K,
+             /24HBOUNDARY EMISSIVITY   =, F12.3,
+             /24HFILTERED RADIANCE   =, 1PE11.3,
+             11H W M-2 SR-1,
+             /24HBLACKBODY TEMPERATURE   =, OPF11.1, 2H C')
+             RADMAX,VRMAX,RADMIN,VRMIN,TBOUND,EMISS,
+             RADSUM, BBTEMP - T0
+         WRITE(IP4,'(T13,F7.2,F8.3,F10.3,F8.3,5(1PE10.3),
+             OPF8.1)')
+             (90.-ANGLE)*pi/180.*1.E3, ANGLE, RANGE,
+             1.-SUMA/Sumf, RADSUM, Nsea, Nsky, Nsun,
+             RADSUM, BBTEMP-T0
+     ELSE
+         WRITE(IPR,'(24H INTEGRATED IRRADIANCE =,1PE11.3,      tras3920
+             10H WATTS M-2,/24H MINIMUM IRRADIANCE   =,E11.3,      tras3930
+             13H WATTS M-2 AT,OPF11.1,5H CM-1,/10H MAXIMUM ,      tras3940
+             14H IRRADIANCE   =,1PE11.3,
+             23H WATTS M-2 (CM-1)-1 AT,OPF11.1,5H CM-1)')
+             RADSUM,RADMIN,VRMIN,RADMAX,VRMAX      tras3960
+         WRITE(IP6,'(
+             24HINTEGRATED IRRADIANCE   =, 1PE11.3, 6H W M-2,
+             /24HMINIMUM IRRADIANCE   =, E11.3,
+             18H W M-2 (CM-1)-1 AT, OPF8.1, 5H CM-1,
+             /24HMAXIMUM IRRADIANCE   =, 1PE11.3,
+             18H W M-2 (CM-1)-1 AT, OPF8.1, 5H CM-1)')
+             RADSUM,RADMIN,VRMIN,RADMAX,VRMAX
+     END IF
+ END IF
C
+ IF (((LastSky) .AND. (IEMSCTold .EQ. 1)) .OR. (SunCard)) THEN
+     WRITE(IP6, '(/, 24HRECEIVED RADIANCE VALUES,
+ //, T10,24H PATH TO FOOTPRINT
+=, F10.5, 11H W M-2 SR-1,
+     T56,12H (AV. TRANS.,          F7.4, 1H),
+     /, T10,24H SEA EMISSION      =, F10.5, 11H W M-2 SR-1,
+     /, T10,24H SKY REFLECTION    =, F10.5, 11H W M-2 SR-1,

```

```

+   /, T10,24H SUN GLINT      =, F10.5, 11H W M-2 SR-1,
+   //, T10,24H TOTAL RADIANCE =, F10.5, 11H W M-2 SR-1,
+   /, T10,24H BLACK BODY TEMP. =, F10.1, 2H C ')
+   Npath, PathTrans, Nsea, Nsky, Nsun, Ntotal, TotalT-T0
+   WRITE(IP4, '(T13,F7.2,F8.3,F10.3,F8.3,5(1PE10.3),0PF8.1)')
+   (90.-PathAngle)*pi/180.*1.E3, PathAngle, PathRange,
+   PathTrans, Npath, Nsea, Nsky, Nsun, Ntotal, TotalT-T0
Npath = 0.
Nsea = 0.
Nsky = 0.
Nsun = 0.
END IF
C
RETURN
END

```

tras4100
tras4110

APPENDIX D
SOURCE CODE FOR NEW *SeaRad* SUBROUTINES

```

***** MOD22.FOR *****
*
* New version of Cox-Munk routines with integration over sea
* slopes and interpolation between three sky angles for estimation
* of incident sky radiance.
*
* Last revised: July 14, 1995.
*
*****
SUBROUTINE Sky(Tr,Pr,W,a,b,v,BoverA,e,Nsky)
REAL Nsky
CU USES rho

C Outputs:
C Calculates (1) the normalization factor "BoverA" in the
C denominator of the interaction probability, and spectral
C values for (2) the effective emmisivity "e" of the ocean
C surface, and (3) the sky radiance "Nsky" [W m-2 sr-1 (cm-1)-1]
C reflected from the ocean surface.

C Inputs:
C The receiver spherical coordinates [rad] are (Tr,Pr). The
C wind speed is W [m s-1]. v [cm-1] is the wavenumber. a and b are
C coefficients of a least squares fit such that Ns, the spectral
C sky radiance [W m-2 sr-1 (cm-1)-1] incident on the ocean
C at zenith angle Ts [rad], is given by

C
C           Ns(Ts,v) = 1./[a(v) - b(v)*Ts**2].
C
C Last revision:
C January 27, 1995.

COMMON/Constants/pi,r2d,d2r,epsilon,delta,onem,onep,infinity
REAL infinity, Ns
if (W .ge. .01) then
    use the Cox-Munk standard deviation for a real sea
    Su = sqrt(3.16E-3*W)
    Sc = sqrt(3.E-3 + 1.92E-3*W)
else
    use a delta function for an ideal calm sea
    Su = .01
    Sc = .01
end if
p0 = 1./(2.*pi*Su*Sc)
Sav = (Su + Sc)/2.
N = 2
M = 7
Smx = N*2.303*Sav
dS = Smx/M
Ar = sin(Tr)*cos(Pr)
Br = sin(Tr)*sin(Pr)
Cr = cos(Tr)

sum1 = 0.
sum2 = 0.
sum3 = 0.

```

```

do Sx = -Smx, Smx, dS
  Symx = sqrt(abs(Smx**2 - Sx**2))
  do Sy = -Symx, Symx, dS
    C           For each position (Sx,Sy) in slope space:
    C           calculate the occurrence probability density p:
    arg = ((Sx/Su)**2 + (Sy/Sc)**2)/2.
    if ((arg) .ge. log(p0/delta)) then
      p = 0.
    else
      p = p0*exp(-arg)
    end if

    C           calculate omega, the angle of incidence and Ts,
    C           the zenith angle of the source ray.
    dd = Sx**2 + Sy**2
    f0 = - Ar*Sx - Br*Sy +Cr
    vv = f0/sqrt(1. + dd)
    if ((onem .le. vv) .and. (vv .le. onep)) then
      omega = 0.
    else if ((-onep .le. vv) .and. (vv .le. -onem)) then
      omega = pi
    else
      omega = acos(vv)
    end if
    uu = (- 2.*Ar*Sx - 2.*Br*Sy + Cr*(1. - dd))/(1. + dd)
    if ((onem .le. uu) .and. (uu .le. onep)) then
      Ts = 0.
    else if ((-onep .le. uu) .and. (uu .le. -onem)) then
      Ts = pi
    else
      Ts = acos(uu)
    end if

    C           interpolate for Ns(Ts),
    Ns = 1./(a - b*(Ts**2))

    C           define integrands,
    f1 = f0*p
    f2 = rho(omega,v)*f1
    f3 = Ns*f2

    C           and accumulate integrals over all slopes.
    if (omega .le. pi/2.) then
      sum1 = f1 + sum1
      sum2 = f2 + sum2
      if (Ts .le. pi/2.) sum3 = f3 + sum3
    end if
    end do
  end do
  sum1 = sum1*dS**2
  sum2 = sum2*dS**2
  sum3 = sum3*dS**2

  BoverA = sum1
  e      = 1. - sum2/sum1

```

```

Nsky    = sum3/sum1

return
END

SUBROUTINE Sun(Tr,Pr,W,To,Po,v,sum4)
CU USES rho

C Outputs:
C     Calculates a spectral solar reflectivity "sum4" for the
C     ocean surface apart from a normalization factor of
C     (4.*"BoverA") or (4.*"sum1").

C Inputs:
C     The receiver spherical coordinates [rad] are (Tr,Pr). The
C     wind speed is W [m s-1]. The spherical coordinates [rad]
C     of the solar center are (To,Po). v [cm-1] is the wavenumber.

C Note:
C     The larger the value of M, the y coordinate step size, the
C     more precise and slower the sum. For fixed M precision
C     improves with wind speed. For W = 1 m s-1 and M = 5, the
C     precision is better than 1.5 % around the center of the
C     glint pattern until the receiver zenith angle exceeds 89.5
C     degrees.

C Bug:
C     Divides by zero when the sun is on the zenith.

C Last Revision:
C     January 27, 1995.

COMMON/Constants/pi,r2d,d2r,epsilon,delta,oneM,oneP,infinity
REAL infinity

C Find the rectangular receiver coordinates
Ar = sin(Tr)*cos(Pr)
Br = sin(Tr)*sin(Pr)
Cr = cos(Tr)

C Find the Cox-Munk wind dependent slope standard deviations
if (W .ge. .01) then
    use the Cox-Munk standard deviation for a real sea
    Su = sqrt(3.16E-3*W)
    Sc = sqrt(3.E-3 + 1.92E-3*W)
else
    use a delta function for an ideal calm sea
    Su = .01
    Sc = .01
end if
p0 = 1./(2.*pi*Su*Sc)

M = 5
N = 2*M + 1
sum = 0.
dy = 2.*epsilon/N
do I = 1, N

```

```

Y      = epsilon - (I - 0.5)*dY
Xmax = sqrt(epsilon**2 - Y**2)
K     = int(2.*Xmax/dY + onem*0.5)
dX   = 2.*Xmax/K
do J = 1, K
    X = Xmax - (J - 0.5)*dX

C      For each position (X,Y) (rectangular coordinates with
C      respect to the solar center) on the solar disk,
C
C      Find the spherical source coordinates:
Ts = To - Y
Ps = Po - X/sin(To)
if (Ts .gt. pi/2.*onep) then
    print *, "Error from 'Sun': Part of solar disk"
    print *, "                                is below horizon."
    return
endif

C      Find the the rectangular source coordinates:
As = sin(Ts)*cos(Ps)
Bs = sin(Ts)*sin(Ps)
Cs = cos(Ts)

C      Find the slopes (Sx,Sy) for a specular reflection from
C      source (Ts,Ps) to receiver (Tr,Pr):
if (abs(As + Ar) .le. delta) then
    Sx = 0.
else if ((Cs + Cr) .le. delta) then
    Sx = sign(infinity, -(As + Ar))
else
    Sx = - (As + Ar)/(Cs + Cr)                               (A12)
end if
if (abs(Bs + Br) .le. delta) then
    Sy = 0.
else if ((Cs + Cr) .le. delta) then
    Sy = sign(infinity, -(Bs + Br))
else
    Sy = - (Bs + Br)/(Cs + Cr)                               (A13)
end if

C      Find the Cox-Munk occurrence probability density:
arg = ((Sx/Su)**2 + (Sy/Sc)**2)/2.
if ((arg) .ge. log(p0/delta)) then
    p = 0.
else
    p = p0*exp(-arg)
end if

C      Find the angle of incidence (omega) for the specular
C      reflection:
dd = (1. + As*Ar + Bs*Br + Cs*Cr)/2.                      (A14)
if (dd .le. delta) dd = 0.
ss = sqrt(dd)                                                 (A14)
if ((onem .le. ss) .and. (ss .le. onep)) then
    omega = 0.
else if ((-onep .le. ss) .and. (ss .le. -onem)) then

```

```

            omega = pi
        else
            omega = acos(ss)
        end if

C      Find the facet tilt (Tn) for the specular reflection:
C      Tn = atan(sqrt(Sx**2 + Sy**2))                                (A14)

C      Integrate:
C      sum = rho(omega,v)/(cos(Tn)**4)*p*dX + sum                  (32)

        end do
    end do
    sum4 = sum*dY
    return
END

SUBROUTINE Fit(x,y,n,a,b)
DIMENSION x(*),y(*)

C      Given (x,y) pairs in the data arrays x(i) and y(i), where
C      1 <= i <= n, performs a least squares fit of these data to
C      the equation

C              y = 1/(a - b*x**2)

C      and returns the values of a and b.

C      Last revised: March 13, 1995.

DOUBLE PRECISION nn, bb, cc(4)
C      where cc(1:4) = c01, c21, c20, c40.
nn = FLOAT(n)

do i = 1, n
    if (y(i) .eq. 0.) then
        a = 7.E5
        b = 0.
        return
    end if
end do

do i = 1, 4
    cc(i) = 0.d0
end do

do i = 1, n
    cc(1) = cc(1) + 1./y(i)
    cc(2) = cc(2) + x(i)**2/y(i)
    cc(3) = cc(3) + x(i)**2
    cc(4) = cc(4) + x(i)**4
end do

bb = (nn*cc(2) - cc(3)*cc(1))/(nn*cc(4) - cc(3)**2)
a = (cc(1) - cc(3)*bb)/nn
b = - bb

```

```
END
```

```
SUBROUTINE Foot(ThetaO, PhiO, ThetaS, PhiS, PsiPO, Beta, Psi)
```

```
USES Angle, Side
```

```
COMMON /Constants/ Spi,Sr2d,Sd2r,epsilon,delta,oneM,oneP,infinity
```

```
COMMON /Geometry/ To,Po,Tr,Pr
```

```
COMMON /Card2/ IHAZE,ISEASN,IVULCN,ICSTL,ICLD,IVSA,VIS,W,WHH,
```

```
+ RAINRT
```

```
COMMON /IFIL/ IRD,IPR,IPU,NPR,IPR1,IP6,IP7,IP8,IP4,IRDS,IP6S,
```

```
+ ITR,Ipath,Isky,Isun
```

```
COMMON /Sea/ Sea, Hit, Msea, TBOUNDold, IEMSCTold
```

```
REAL infinity
```

```
C
```

```
*****
```

```
*
```

```
* This routine calculates zenith angles and azimuthal angles from *
```

```
* the footprint, defined as the location where a hit has just *
```

```
* occurred.
```

```
*
```

```
* All the arguments are inputs, and all are angles in degrees:
```

```
* ThetaO and PhiO are the observer latitude and longitude.
```

```
* ThetaS and PhiS are the solar latitude and longitude.
```

```
* PsiPO is the path azimuth (+ E of N) seen by the observer.
```

```
* Beta is the angle subtended at the center of the earth
```

```
* between the observer and the footprint.
```

```
* PsiW is the wind azimuth (+E of N) seen by the observer.
```

```
*
```

```
* The outputs are To, Po, and Pr, angles in radians passed *
```

```
* through the common block "Geometry":
```

```
* To is the zenith angle of the center of the sun *
```

```
* from the footprint.
```

```
* Po is the azimuth (+ W. of PsiW) of the center of the sun *
```

```
* from the footprint.
```

```
* Pr is the azimuth (+ W. of PsiW) receiver as seen *
```

```
* from the footprint.
```

```
* Note: Tr has been calculated in DPPNMN and is used *
```

```
* in this subroutine only for printing to "OUT".
```

```
*
```

```
* Last revision: June 15, 1995.
```

```
*
```

```
*****
```

```
DOUBLE PRECISION DThetaO, DPhiO, DThetaS, DPhiS, DPSiPO, DBeta,
```

```
+ DPSiW, DThetaF, DPhiF, Pi, Side, Angle, DTo, DPo
```

```
Pi = 4.*DATAN(1.)
```

```
D2R = Pi/180.
```

```
R2D = REAL(180./Pi)
```

```
C
```

```
First, convert to radians and increase precision:
```

```
DThetaS = DBLE(ThetaS)*D2R
```

```
DPhiS = DBLE(PhiS)*D2R
```

```
DThetaO = DBLE(ThetaO)*D2R
```

```
DPhiO = DBLE(PhiO)*D2R
```

```
DPSiPO = DBLE(PsiPO)*D2R
```

```
DBeta = DBLE(Beta)*D2R
```

```

DPsiW    = DBLE(Psi+PsiPO)*D2R
C      then use the geometry of three spherical triangles connecting
C      the north pole, the observer, and the footprint:
DThetaF = Pi/2. - Side(Pi/2.-DThetaO, -DPsiPO, DBeta)

IF (DPsiPO .GE. Pi) THEN
    DPhiF = DPhiO + Angle(Pi/2.-DThetaO,DBeta,Pi/2.-DThetaF)
ELSE
    DPhiF = DPhiO - Angle(Pi/2.-DThetaO,DBeta,Pi/2.-DThetaF)
END IF

DTo = Side(Pi/2.-DThetaS, DPhiS-DPhiF, Pi/2.-DThetaF)
To = REAL(DTo)

IF (DPhiS .GE. DPhiO) THEN
    DPo = DPsiW + Angle(Pi/2.-DThetaF, Pi/2.-DThetaS, DTo)
ELSE
    DPo = DPsiW - Angle(Pi/2.-DThetaF, Pi/2.-DThetaS, DTo)
END IF
Po = REAL(DPo)

IF (DPhiF .GE. DPhiO) THEN
    DPr = DPsiW - Angle(Pi/2.-DThetaF, Pi/2.-DThetaO, DBeta)
ELSE
    DPr = DPsiW + Angle(Pi/2.-DThetaF, Pi/2.-DThetaO, DBeta)
END IF
Pr = REAL(DPr)

C      Calculate specular slope (merely for print-out, not used for
C      further calculations):

C      Find the rectangular receiver coordinates,
Ar = sin(Tr)*cos(Pr)
Br = sin(Tr)*sin(Pr)
Cr = cos(Tr)

C      Find the the rectangular source coordinates for the solar center,
Ao = sin(To)*cos(Po)
Bo = sin(To)*sin(Po)
Co = cos(To)

C      Find the Cox-Munk wind dependent slope variances
if (W .ge. .01) then
    use the Cox-Munk variance for a real sea
    Vu = 0.000 + 3.16E-3*W
    Vc = 0.003 + 1.92E-3*W
else
    use a delta function for an ideal calm sea
    Vu = .0001
    Vc = .0001
end if
p0 = 1./(2.*pi*sqrt(Vu*Vc))

C      Find the slopes (Sxo,Syo) for a specular reflection from
C      source (To,Po) to receiver (Tr,Pr),

```

```

if (abs(Ao + Ar) .le. delta) then
    Sxo = 0.
else if ((Co + Cr) .le. delta) then
    Sxo = sign(infinity, -(Ao + Ar))
else
    Sxo = - (Ao + Ar)/(Co + Cr)                                (A12)
end if
if (abs(Bo + Br) .le. delta) then
    Syo = 0.
else if ((Co + Cr) .le. delta) then
    Syo = sign(infinity, -(Bo + Br))
else
    Syo = - (Bo + Br)/(Co + Cr)                                (A13)
end if

C   Calculate the Cox-Munk tilt and slope:
arg = Sxo**2/Vu + Syo**2/Vc
p  = p0*exp(-0.5*arg)
Tn = atan(sqrt(Sxo**2 + Syo**2))

C   and print to "OUT":
WRITE (IP6,1000)
WRITE (IP6,1010) DBeta*R2D,DPsiPO*R2D,AMOD(DPsiW*R2D,360.)
IF ((IEMSCToId) .EQ. 2) THEN
    WRITE (IP6,1020) DThetaO*R2D,DPhiO*R2D,DThetaF*R2D,DPhiF*R2D,
+                  DThetaS*R2D,DPhiS*R2D
END IF
WRITE (IP6,1030)
WRITE (IP6,1040) Tr*R2D,AMOD(Pr*R2D,360.)
IF ((IEMSCToId) .EQ. 2) THEN
    WRITE (IP6,1050) To*R2D,AMOD(Po*R2D,360.),Sr2d*Tn,sqrt(arg),p
END IF

C
1000 format(//,'SUMMARY OF OBSERVATION GEOMETRY')
1010 format (10X,'BETA          =' ,F10.5,
+           ' DEG',//,
+           10X,'PATH AZIMUTH      =' ,F10.3,
+           ' DEG EAST OF NORTH',//,
+           10X,'WIND AZIMUTH      =' ,F10.3,
+           ' DEG EAST OF NORTH',\)
1020 format (10X,'RECEIVER LATITUDE     =' ,F10.3,
+           ' NORTH OF EQUATOR',//,
+           10X,'RECEIVER LONGITUDE    =' ,F10.3,
+           ' WEST OF GREENWICH',//,
+           10X,'FOOTPRINT LATITUDE    =' ,F10.3,
+           ' NORTH OF EQUATOR',//,
+           10X,'FOOTPRINT LONGITUDE   =' ,F10.3,
+           ' WEST OF GREENWICH',//,
+           10X,'SUBSOLAR LATITUDE    =' ,F10.3,
+           ' DEG NORTH OF EQUATOR',//,
+           10X,'SUBSOLAR LONGITUDE   =' ,F10.3,
+           ' DEG WEST OF GREENWICH',//)
1030 format(//,'VALUES SEEN FROM FOOTPRINT')
1040 format (10X,'RECEIVER ZENITH ANGLE =' ,F10.3,
+           ' DEG',//,
+           10X,'RECEIVER AZIMUTH      =' ,F10.3,

```

```

+           ' DEG WEST OF UP WIND')
1050 format (10X,'SOLAR ZENITH ANGLE      =',F10.3,
+           ' DEG',/,
+           10X,'SOLAR AZIMUTH      =',F10.3,
+           ' DEG WEST OF UP WIND',/,
+           10X,'SOLAR SPECULAR TILT =',F10.3,
+           ' DEG (', F6.2, ' SIGMA, PROB =',1PE10.3,')')

      return
      END

      SUBROUTINE SunFoot(Psi0, Del0, PsiPO, Beta, Psi)
CU      USES Angle, Side
      COMMON /Constants/ Spi,Sr2d,Sd2r,epsilon,delta,oneM,oneP,infinity
      COMMON /Geometry/ To,Po,Tr,Pr
      COMMON /Card2/ IHAZE,ISEASN,IVULCN,ICSTL,ICLD,IVSA,VIS,W,WHH,
+                   RAINRT
      COMMON /IFIL/ IRD,IPR,IPU,NPR,IPR1,IP6,IP7,IP8,IP4,IRDS,IP6S,
+                   ITR,Ipath,Isky,Isun
      COMMON /Sea/ Sea, Hit, Msea, TBOUNDold, IEMSCTold
      REAL infinity
C
*****
*
* This routine calculates zenith angles and azimuthal angles from
* the footprint, defined as the location where a hit has just
* occurred, whenever the sun is involved. (PsiPO is not used in
* the calculation; it's passed in only to be printed out.)
*
* All the arguments are inputs, and all are angles in degrees:
* Psi0 is the solar azimuth measured from the observer's
*     line-of-sight (+E of N).
* Del0 is the solar zenith angle as seen by the observer.
* Beta is the angle subtended at the center of the earth
*     between the observer and the footprint.
* Psi is the wind azimuth measured from the observer's
*     line-of-sight (+E of N).
*     (Psi is ASSUMED to be the same at the footprint.)
*
* The outputs are To, Po, and Pr, angles in radians passed
* through the common block "Geometry":
*     To is the zenith angle of the center of the sun
*         from the footprint.
*     Po is the azimuth (+ W of PsiW) of the center of the sun
*         from the footprint.
*     Pr is the azimuth (+ W of PsiW) receiver as seen
*         from the footprint.
* Note: Tr has been calculated in DPFNMN and is used
*         in this subroutine only for printing to "OUT".
*
* Last revision: June 14, 1995.
*
*****
      DOUBLE PRECISION DPsi0, DDel0, DBeta, Pi, Side, Angle, DTo, DPr
      Pi = 4.*DATAN(1.)

```

```

D2R = Pi/180.
R2D = REAL(180./Pi)

C First, convert to radians and increase precision:

DPsi0 = DBLE(Psi0)*D2R
DDel0 = DBLE(Del0)*D2R
DBeta = DBLE(Beta)*D2R
DPsi = DBLE(Psi)*D2R

C then use the geometry of the spherical triangle connecting
C the observer, the sun, and the footprint:

DTO = Side(DBeta, DPsi0, DDel0)
To = REAL.DTO

DPr = Pi + DPsi
Pr = REAL(DPr)

If (DPsi0 .GT. 0.) then
    DPo = DPr + Angle.DTO, DDel0, DBeta)
Else if (DPsi0 .EQ. 0.) then
    DPo = DPr + Pi
Else
    DPo = DPr - Angle.DTO, DDel0, DBeta)
End If
Po = REAL(DPo)

C Calculate specular slope (calculations from now on merely for
C print-out, not for further calculations):

C Find the rectangular receiver coordinates,
Ar = sin(Tr)*cos(Pr)
Br = sin(Tr)*sin(Pr)
Cr = cos(Tr)

C Find the the rectangular source coordinates for the solar center,
Ao = sin(To)*cos(Po)
Bo = sin(To)*sin(Po)
Co = cos(To)

C Find the Cox-Munk wind dependent slope variances
if (W .ge. .01) then
    use the Cox-Munk variance for a real sea
    Vu = 0.000 + 3.16E-3*W
    Vc = 0.003 + 1.92E-3*W
else
    use a delta function for an ideal calm sea
    Vu = .0001
    Vc = .0001
end if
p0 = 1./(2.*pi*sqrt(Vu*Vc))

C Find the slopes (Sxo,Syo) for a specular reflection from
C source (To,Po) to receiver (Tr,Pr),
if (abs(Ao + Ar) .le. delta) then
    Sxo = 0.

```

```

        else if ((Co + Cr) .le. delta) then
            Sxo = sign(infinity, -(Ao + Ar))
        else
            Sxo = - (Ao + Ar)/(Co + Cr)
        end if
        if (abs(Bo + Br) .le. delta) then
            Syo = 0.
        else if ((Co + Cr) .le. delta) then
            Syo = sign(infinity, -(Bo + Br))
        else
            Syo = - (Bo + Br)/(Co + Cr)
        end if
    end if
    C Calculate the Cox-Munk tilt and slope:
    arg = Sxo**2/Vu + Syo**2/Vc
    p = p0*exp(-0.5*arg)
    Tn = atan(sqrt(Sxo**2 + Syo**2))

    C and print to "OUT":
    WRITE (IP6,2000)
    WRITE (IP6,2010) DBeta*R2D,PsiPO,AMOD((Psi+PsiPO), 360.)
    WRITE (IP6,2030)
    WRITE (IP6,2040) Tr*R2D,AMOD(Pr*R2D,360.)
    IF ((IEMSCTold) .EQ. 2) THEN
        WRITE (IP6,2050) To*R2D,AMOD(Po*R2D,360.),Sr2d*Tn,sqrt(arg),p
    END IF
    C
    2000 format(/, 'SUMMARY OF OBSERVATION GEOMETRY')
    2010 format (10X,'BETA'           ='',F10.5,
    +          ' DEG',//,
    +          10X,'PATH AZIMUTH      ='',F10.3,
    +          ' DEG EAST OF NORTH',//,
    +          10X,'WIND AZIMUTH      ='',F10.3,
    +          ' DEG EAST OF NORTH',\)
    2030 format(/, 'VALUES SEEN FROM FOOTPRINT')
    2040 format (10X,'RECEIVER ZENITH ANGLE ='',F10.3,
    +          ' DEG',//,
    +          10X,'RECEIVER AZIMUTH     ='',F10.3,
    +          ' DEG WEST OF UP WIND')
    2050 format (10X,'SOLAR ZENITH ANGLE   ='',F10.3,
    +          ' DEG',//,
    +          10X,'SOLAR AZIMUTH       ='',F10.3,
    +          ' DEG WEST OF UP WIND',//,
    +          10X,'SOLAR SPECULAR TILT  ='',F10.3,
    +          ' DEG (', F6.2, ' SIGMA, PROB =',1PE10.3,')')

    return
END

SUBROUTINE Card
COMMON /Card2/ IHAZE,ISEASN,IVULCN,ICSTL,ICLD,IVSA,VIS,WSS,WHH,
+              RAINRT
COMMON /Card3/ H1,H2,ANGLE,RANGE,BETA,RE,LEN,Psi,SeaSwitch
COMMON /Card3A1/ IPARM,IPH,IDAY,ISOURC
COMMON /Card3A2/ PARM1,PARM2,PARM3,PARM4,GMT,PSIPO,ANGLEM,G
COMMON /IFIL/ IRD,IPR,IPU,NPR,IPR1,IP6,IP7,IP8,IP4,IRDS,IP6S,

```

```

+           ITR,Ipath,Isky,Isun
COMMON /Constants/ pi,r2d,d2r,epsilon,delta,onem,onep,infinity
COMMON /Geometry/ To,Po,Tr,Pr
COMMON /Sea/ Sea,Hit,Msea,TBOUNDold,IEMSCTold
REAL infinity
LOGICAL SeaSwitch

*****
* Issues new MODTRAN cards for the sea routines.
*
* When IEMSCTold = 1, no sun is involved, and three new sky
* cards are issued to "TAPE5.SEA": one for Tmin, the minimum sky
* zenith angle expected at the current wind speed, one for
* for Tmax, the maximum zenith angle expected, and one for Tav,
* the sky zenith angle halfway between Tmax and Tmin.
*
* When IEMSCTold = 2, the sun is involved, and after each new sky
* card the original cards 3A1 and 3A2 are reissued. At the very
* end of the file there is one sun card. Hence the number of new
* cards issued to 'TAPE5.SEA' is 10 when IEMSCTold = 2.
*
* Last revised: February 28, 1995.
*
*****
Irpt = 3

C First, find the wind-dependent sky angles Tmin and Tmax:
if (WSS .ge. .01) then
  use the Cox-Munk standard deviation for a real sea
  Su = sqrt(3.16E-3*WSS)
  Sc = sqrt(3.E-3 + 1.92E-3*WSS)
else
  use a delta function for an ideal calm sea
  Su = .01
  Sc = .01
end if
S = 2.8
is the number of standard deviations to which the
wave slope integral will be carried; for S = 2.8
99 % of the volume under the distribution is captured.
dT = 2.02*(atan(S*amax1(Su,Sc)))
Tmin = amax1(Tr - dT, 1.)
Tmax = amin1(Tr + dT, d2r*89.)

C Next, open TAPE5.SEA, the alternate file to TAPE5:
open (Irds, file = 'Tape5.Sea', status = 'unknown')

C then write the sky cards (IEMSCT = 2, ITYPE = 3):
do Ts = Tmin, Tmax, onem*(Tmax-Tmin)/2.
  write (Irds, 150) Irpt
  write (Irds, 100) 0.,0.,Ts*r2d,0.,0.,0.,0.,Psi,SeaSwitch
  if (IEMSCTold .eq. 2) then
    write (Irds, 400) IPARM,IPH,IDADY,ISOURC
    write (Irds, 500) PARM1,PARM2,PARM3,PARM4,GMT,PSIPO,
+                               ANGLEM,G

```

```

        end if
end do

C   write the sun card (IEMSCT = 3, ITYPE = 3) if necessary:
if (IEMSCTold .EQ. 2) then
    write (Irds, 150) Irpt
    write (Irds, 200) 0.,0.,To*r2d, IDAY, 0.,0,0.
end if

C   and finally
rewind Irds
C   so it can be read from the beginning by the driver.

return

100 format (6F10.3,I5,F10.3,L5)
150 format (I5)
200 format (3F10.3,I5,5X,F10.3,I5,F10.3)
400 format (4I5)
500 format (8F10.3)

END

***** FUNCTIONS *****
*
*   Latest revision: May 5, 1994 for Side and Angle.
*
***** FUNCTIONS *****

FUNCTION Side(a,C,b)
C   is the Law of Cosines for a spherical triangle with sides a, b,
C   and c and opposite angles A, B, C. The three parameters are
C   the two sides a and b and the included angle C. Side is the
C   value of side c opposite the included angle C. Angles are in
C   radians.

double precision a,C,b,Side
Side = dacos(dcos(a)*dcos(b) + dsin(a)*dsin(b)*dcos(C))
END

FUNCTION Angle(a,c,b)
C   is the Law of Cosines for a spherical triangle with sides a, b,
C   and c and opposite angles A, B, C. The three parameters are
C   the three sides. Angle is the value of angle C opposite side
C   c, the middle parameter in the list. Angles are in radians.

double precision pi,a,b,c,Angle,Arg,aa,bb
pi = 4.*datan(1.)
aa = dmin1(a, b)
bb = dmax1(a, b)

if (abs(aa) .le. 1.D-5) then
    Angle = dacos(dtan(aa)/dtan(bb))
    if (abs(bb) .lt. abs(c)) Angle = pi - Angle
end if

```

```

Arg = (dcos(c) - dcos(a)*dcos(b))/(dsin(a)*dsin(b))
if (abs(Arg) .ge. (1 - 1.D-14)) then
    Angle = 0.
else
    Angle = dacos(Arg)
end if

END

FUNCTION Rho(Omega, V)
CU   USES SeaData
COMMON /SeaIndex/ Alpha01(100), Alpha02(20),
+                 Beta01 (100), Beta02 (20)

*****
*      Calculates reflectivity of sea water between 52.63 cm-1 and
* 25,000 cm-1 using equations (74) and (78) of Stratton, "Electro-
* magnetic Theory", 1941, page 505, ff. The sea water is assumed to
* be a conducting medium; both real and imaginary parts of the
* index of water are used. The notation of Stratton is adhered to
* as closely as possible.
*
*      Omega is the angle of incidence in radians; V is the wave-
* number in cm-1; Rho is the reflectivity.
*
* Last revision: November 28, 1994
*
*****
```

C The four-point interpolation functions are:

```

WM(X) = (X - 1.)*(X - 2.)*X/6.
W0(X) = (X - 1.)*(X - 2.)*(X + 1.)/2.
W1(X) = (X + 1.)*(X - 2.)*X/2.
W2(X) = (X + 1.)*(X - 1.)*X/6.
```

C IF ((Omega .LT. 0.) .OR. (Omega .GT. 1.57080)) THEN
C Omega is out of bounds; set reflectivity to 0% and return:

```

Rho = 0.
RETURN
END IF
```

C IF (V .EQ. 0.) THEN
C set reflectivity to 100% and return:

```

Rho = 1.
RETURN
END IF
```

W = 1.E4/V

C IF (W .LT. 0.399999) THEN
C print error message and return:

```

Rho = 0.
WRITE (6, 1000) V
RETURN
END IF
```

```

C      IF (0.4 .LE. W .AND. W .LE. 19.8) THEN
C      use Lagrange 4 point interpolation on Block 01 data which
C      are at 0.2 um spacing between 0.2 and 20 um:
C          I = INT(W/0.2)
C          Fr = MOD(W, 0.2)/0.2
C          Alpha1 = W2(Fr)*Alpha01(I + 2) - W1(Fr)*Alpha01(I + 1)
C          +     + W0(Fr)*Alpha01(I)      - WM(Fr)*Alpha01(I - 1)
C          Beta1 = W2(Fr)*Beta01 (I + 2) - W1(Fr)*Beta01 (I + 1)
C          +     + W0(Fr)*Beta01 (I)      - WM(Fr)*Beta01 (I - 1)
C      END IF

C      IF (19.8 .LT. W .AND. W .LT. 190.) THEN
C      use Lagrange 4 point interpolation on Block 02 data which
C      are at 10 um spacing between 10 and 200 um:
C          I = INT(W/10.)
C          Fr = MOD(W, 10.)/10.
C          Alpha1 = W2(Fr)*Alpha02(I + 2) - W1(Fr)*Alpha02(I + 1)
C          +     + W0(Fr)*Alpha02(I)      - WM(Fr)*Alpha02(I - 1)
C          Beta1 = W2(Fr)*Beta02 (I + 2) - W1(Fr)*Beta02 (I + 1)
C          +     + W0(Fr)*Beta02 (I)      - WM(Fr)*Beta02 (I - 1)
C      END IF

C      IF (190. .LE. W) THEN
C          print error message and return:
C              RHO = 0.
C              WRITE (6, 1000) V
C              RETURN
C      END IF

C      G = Alpha1**2 - Beta1**2 - SIN(Omega)**2
C      H = 4*(Alpha1**2)*(Beta1**2)
C      P = SQRT(0.5*(-G + SQRT(H + G**2)))
C      Q = SQRT(0.5*(+G + SQRT(H + G**2)))

C      Stratton, Equation (74), p. 505:
C      C = (Q - COS(Omega))**2 + P**2
C      D = (Q + COS(Omega))**2 + P**2
C      Rp = C/D

C      Stratton, Equation (77), p. 506:
C      E = ((Alpha1**2 - Beta1**2)*COS(Omega) - Q)**2
C      F = ((Alpha1**2 - Beta1**2)*COS(Omega) + Q)**2
C      T = (2*Alpha1*Beta1*COS(Omega) - P)**2
C      U = (2*Alpha1*Beta1*COS(Omega) + P)**2
C      Rs = (E + T)/(F + U)

C      Rho = (Rp + Rs)/2.

C      RETURN
1000 FORMAT (' ***** WARNING - INPUT FREQUENCY = ', 1PG12.5, 'CM-1',
+           ', ' OUTSIDE VALID RANGE OF 52.63 TO 25,000 CM-1 *****',/)
END

BLOCK DATA SeaData
COMMON /SeaIndex/ Alpha01(100), Alpha02(20),
+                   Beta01 (100), Beta02 (20)

```

```
*****
* These data for the optical index of water have been taken from *
* the literature. From 0.2 to 2 microns (blocks 01 up to second *
* entry of row B) and from 10 to 200 microns (blocks 02) the data *
* are from G. M. Hale and M. R. Querry, "Optical Constants of Water*
* in the 200-nm to 200- $\mu$ m Wavelength Region," Appl. Opt. 3, 555 *
* (1973). These data are for pure water. *
* 
```

```
* From 2.2 to 20 microns (blocks 01 from the third entry of row B *
* to the end) the data are from M. R. Querry, W. E. Holland, R. C. *
* Waring, L. M. Earls, and M. D. Querry, "Relative Reflectance and *
* Complex Refractive Index in the Infrared for Saline Environmental*
* Waters," J. Geophys. Res. 82, 1425 (1977), Table 3, Pacific *
* Ocean columns. These data are for salt water. *
* 
```

```
*****
C Real part of the index of sea water from 0.2 to 20 microns in
C steps of 0.2 microns:
```

```
DATA Alpha01 /
A 1.396, 1.339, 1.332, 1.329, 1.327, 1.324, 1.321, 1.317,
B 1.312, 1.306, 1.303, 1.287, 1.251, 1.151, 1.384, 1.479,
C 1.421, 1.388, 1.368, 1.355, 1.347, 1.339, 1.335, 1.335,
D 1.332, 1.324, 1.312, 1.296, 1.268, 1.271, 1.371, 1.353,
E 1.340, 1.330, 1.324, 1.319, 1.314, 1.307, 1.302, 1.297,
F 1.291, 1.286, 1.279, 1.272, 1.268, 1.264, 1.258, 1.249,
G 1.240, 1.229, 1.218, 1.204, 1.190, 1.177, 1.165, 1.151,
H 1.140, 1.132, 1.124, 1.119, 1.121, 1.126, 1.134, 1.142,
I 1.152, 1.164, 1.177, 1.189, 1.201, 1.212, 1.224, 1.234,
J 1.242, 1.253, 1.261, 1.273, 1.284, 1.296, 1.309, 1.320,
K 1.331, 1.339, 1.349, 1.358, 1.366, 1.379, 1.390, 1.399,
L 1.408, 1.417, 1.426, 1.435, 1.443, 1.450, 1.458, 1.464,
M 1.470, 1.474, 1.477, 1.480 /
```

```
C Real part of the index of sea water from 10 to 200 microns in
C steps of 10 microns:
```

```
DATA Alpha02 /
A 1.218, 1.480, 1.551, 1.519, 1.587, 1.703, 1.821, 1.886,
B 1.924, 1.957, 1.966, 2.004, 2.036, 2.056, 2.069, 2.081,
C 2.094, 2.107, 2.119, 2.130 /
```

```
C Imaginary part of the index of sea water from 0.2 to 20 microns in
C steps of 0.2 microns:
```

```
DATA Beta01 /
A 0.000, 0.000, 0.000, 0.000, 0.000, 0.000, 0.000, 0.000,
B 0.000, 0.001, 0.000, 0.001, 0.003, 0.114, 0.263, 0.085,
C 0.018, 0.005, 0.003, 0.004, 0.007, 0.011, 0.016, 0.016,
D 0.013, 0.011, 0.010, 0.013, 0.032, 0.108, 0.087, 0.044,
E 0.035, 0.033, 0.032, 0.031, 0.031, 0.032, 0.032, 0.033,
F 0.034, 0.036, 0.038, 0.041, 0.044, 0.046, 0.046, 0.047,
G 0.048, 0.050, 0.054, 0.060, 0.068, 0.079, 0.091, 0.107,
H 0.125, 0.145, 0.166, 0.191, 0.216, 0.239, 0.260, 0.279,
I 0.297, 0.313, 0.326, 0.338, 0.347, 0.357, 0.363, 0.371,
J 0.377, 0.385, 0.393, 0.401, 0.407, 0.413, 0.417, 0.418,
K 0.420, 0.422, 0.424, 0.427, 0.430, 0.432, 0.432, 0.432,
L 0.431, 0.430, 0.429, 0.427, 0.425, 0.423, 0.420, 0.416,
```

```
M      0.414, 0.410, 0.406, 0.393  /  
C      Imaginary part of the index of sea water from 10 to 200 microns in  
C      steps of 10 microns:  
DATA Beta02  /  
A      0.051, 0.393, 0.328, 0.385, 0.514, 0.587, 0.576, 0.547,  
B      0.536, 0.532, 0.531, 0.526, 0.514, 0.500, 0.495, 0.496,  
C      0.497, 0.499, 0.501, 0.504  /  
END
```